

Prethodno napregnute konstrukcije

Predavanja
2021/2022

PIV – Sistemi i tehnologija

Tehnologija i postupci prethodnog naprezanja

Prethodno naprezanje prethodnim zatezanjem – na stazi



Na kraju staze za prethodno naprezanje postavljene su hidrauličke prese za zatezanje užadi



Hidrauličke prese rade na principu pritiska ulja. Sila koja se aplicira presom mjeri se pomoću mjerača pritiska ulja ili posebnog mjerača sile.

Redoslijed operacija pri prethodnom naprezanju na stazi

1 Sidrenje užadi, postavljanje presa, zatezanje čelika

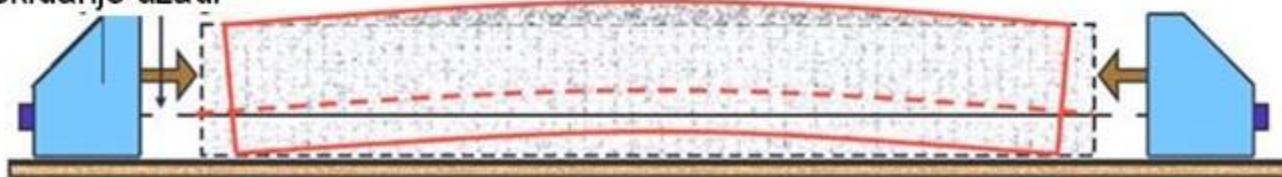


2. Betoniranje konstruktivnog elementa



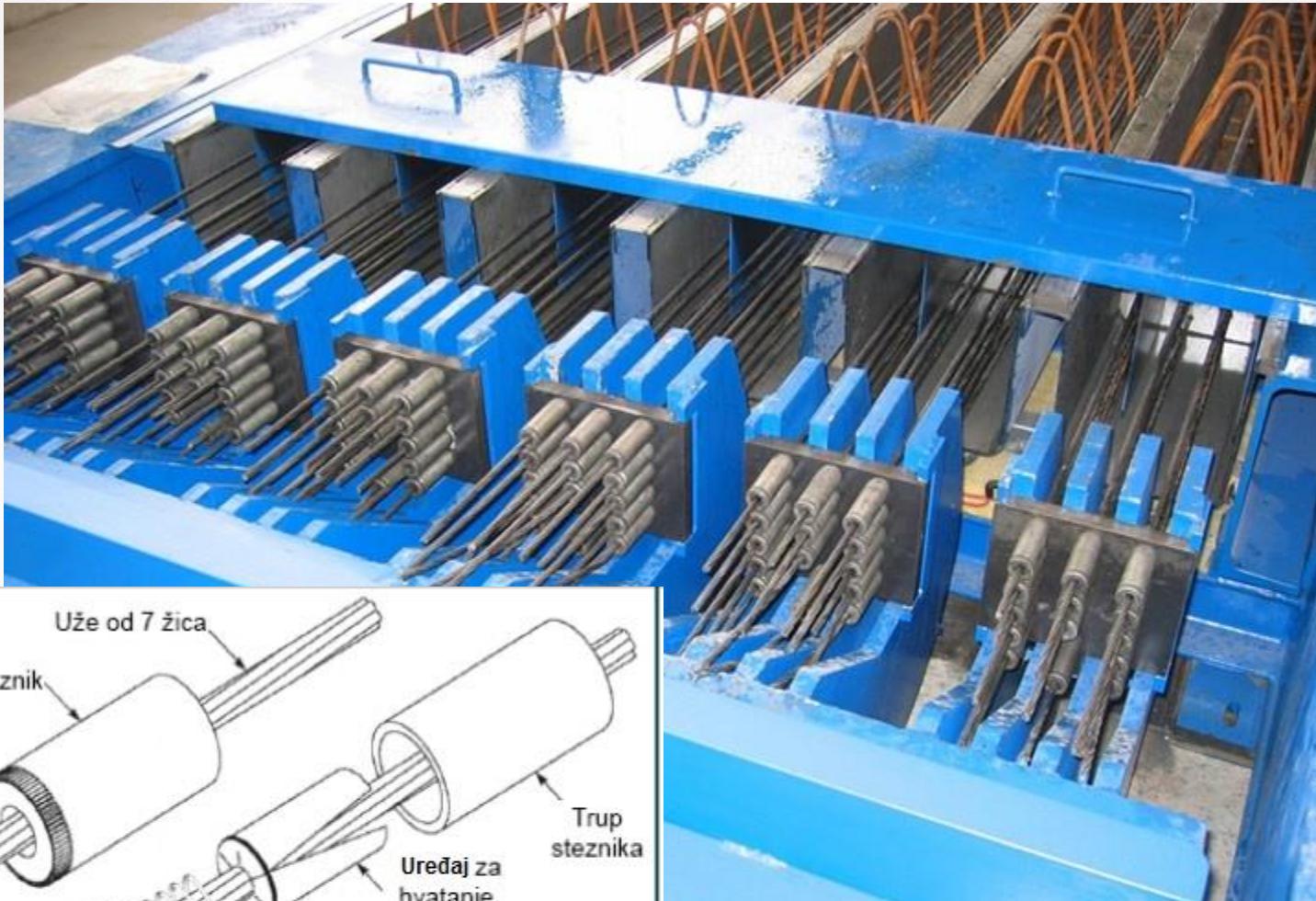
3 Otpuštanje užadi i prenos naprezanja

Prekidanje užadi



Nakon prenosa naprezanja sa užadi na beton dolazi do elastičnog skraćenja elementa.
Ukoliko su kablovi postavljeni ekscentrično element će dobiti negativan ugib - nadvišenje.

Sidrenje kod prethodnog naprezanja na stazi

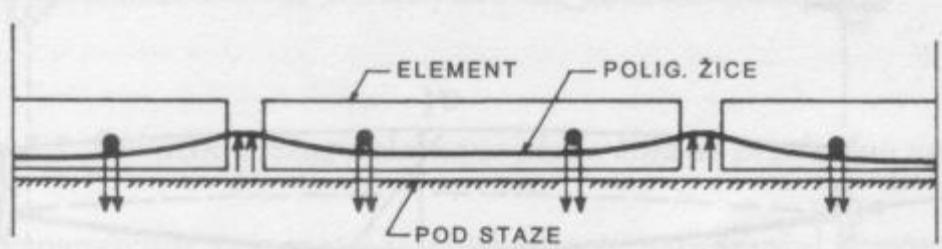


Koriste se uređaji za sidrenje koji se jednostavno otpuštaju

Staza za prethodno naprezanje sa postavljenim užadima i mekom armaturom

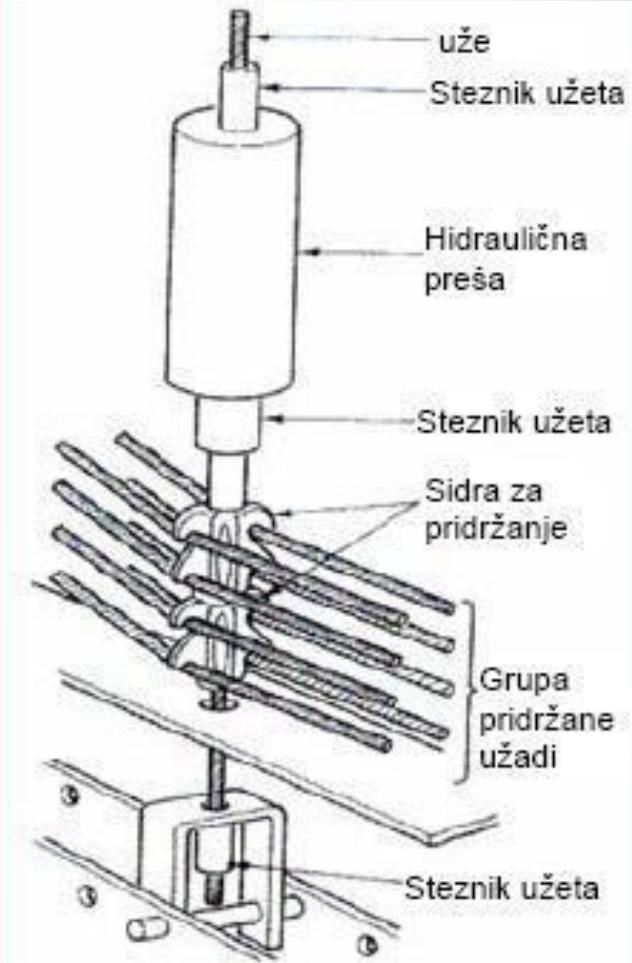
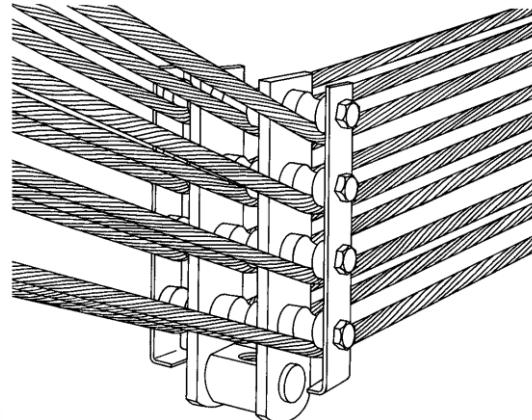
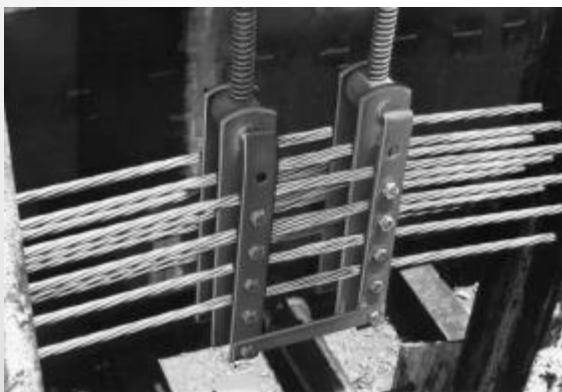
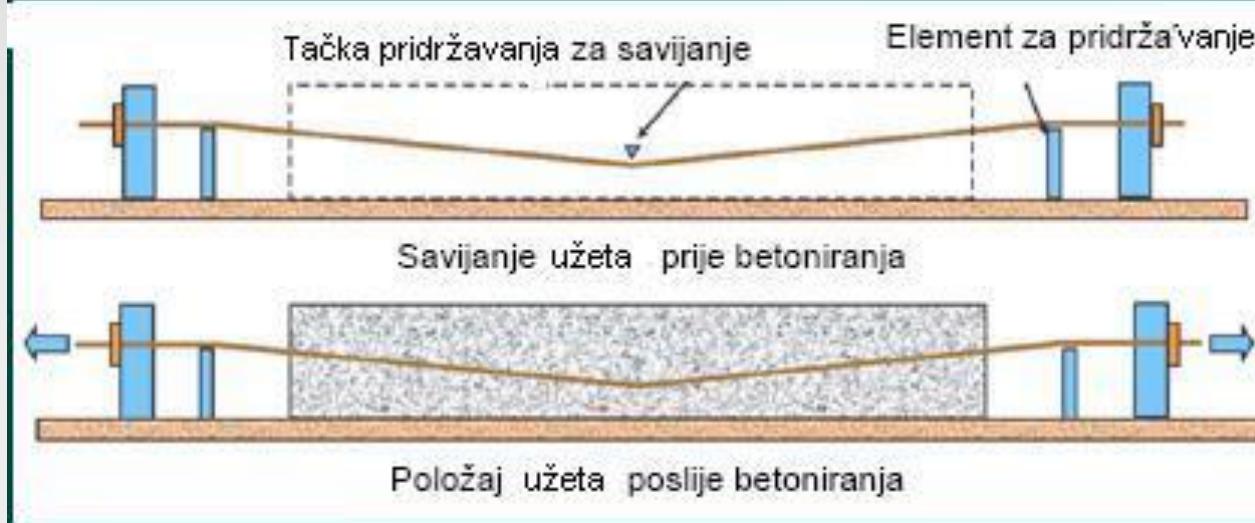


Kod elemenata prethodno napregnutih na stazi često se predviđa postavljanje užadi (žica) po poligonalnoj trasi.



Poligonalni tok užadi (žica) je poželjan u cilju boljeg prilagođavanja efekata prethodnog naprezanja konstruktivnim uslovima.

Užad se usmjeravaju po predviđenoj trasi korišćenjem posebnih uređaja za pridržavanje užadi.

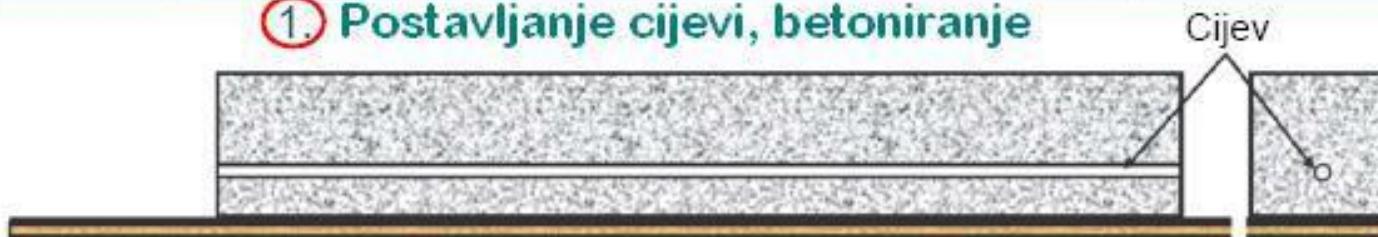


Uredaji za pridržavanje (skretanje) užadi

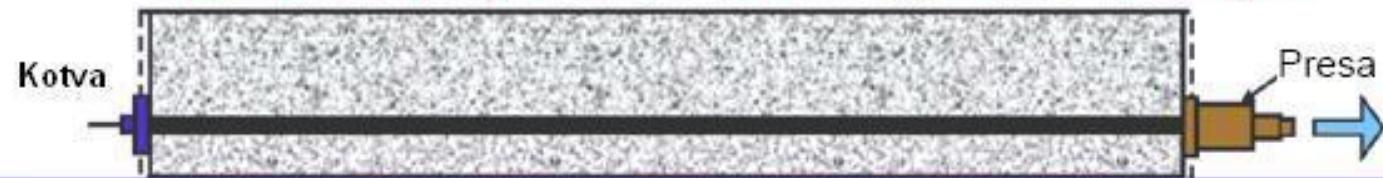
Prethodno naprezanje naknadnim zatezanjem

Redoslijed operacija

1. Postavljanje cijevi, betoniranje



2. Postavljanje kablova, kotve i prese, zatezanje



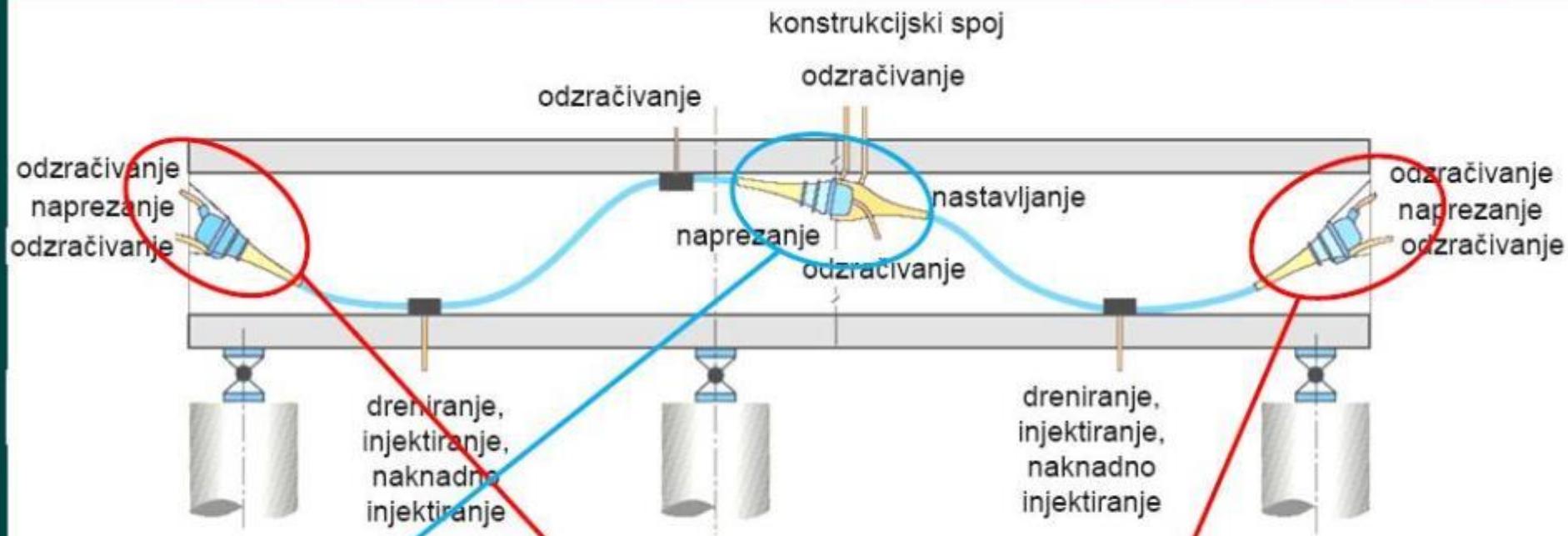
3. Ankerovanje na slobodnom kraju



Operacije i postupci pri prethodnom naprezanju naknadnim zatezanjem

- ❖ U betonskom elementu se postavljaju zaštitne cijevi duž projektovane putanje – trase kablova
- ❖ Kroz otvore (cijevi) se provlače kablovi za prethodno naprezanje
- ❖ Zatezanje kablova se vrši nakon očvršćavanja betona
- ❖ Ankerovanje kablova se vrši pomoću kotvi
- ❖ Kotve mogu biti fiksne i pokretnе
- ❖ Fiksna kotva može biti na jednom kraju, dok na drugom mora biti pokretna, za zatezanje kabla. Moguće je postaviti pokretnе kotve na oba kraja kabla.
- ❖ Nakon zatezanja i ankerovanja kablova vrši se injektiranje – popunjavanje prostora između cijevi i kabla radi zaštite kabla od korozije i monolitizacije presjeka

Djelovi sistema za naknadno zatezanje

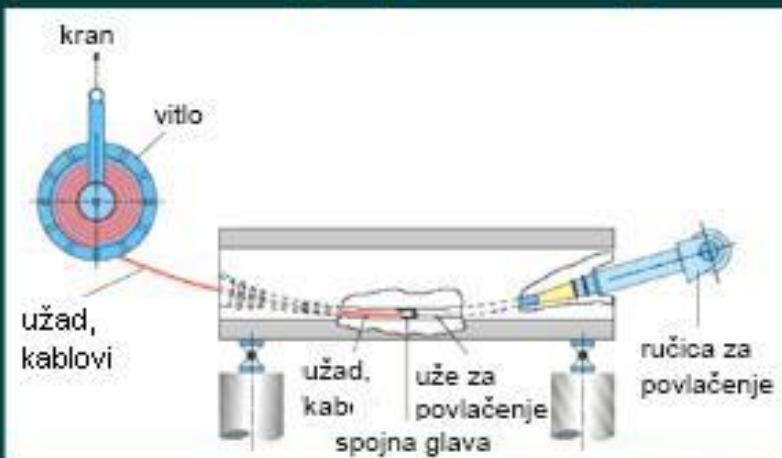


DYWIDAG

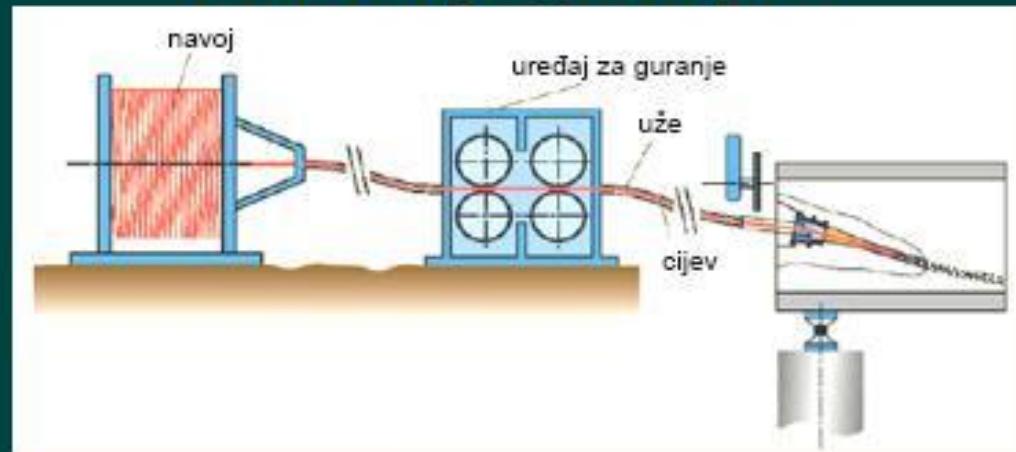


Uvlačenje kablova - užadi

Uvlačenje potezanjem



Uvlačenje guranjem



Zatezanje kablova vrši se pomoću hidrauličkih presa.



Presa Jack HoZ 4,000

Presu zajedno sa hidrauličkom pumpom služi za zatezanje kablova.

Kapacitet prese DYWIDAG je od 250-9750kN.

Hidrauličkom pumpom se kontroliše pritisak ulja u presi, na kojoj postoji ventil za zaštitu od preopterećenja.

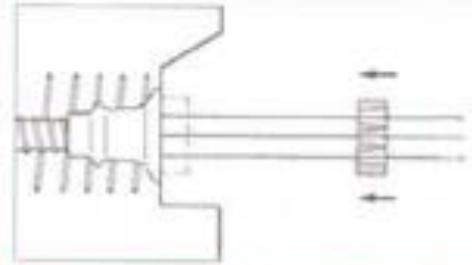
Hidraulička pumpa



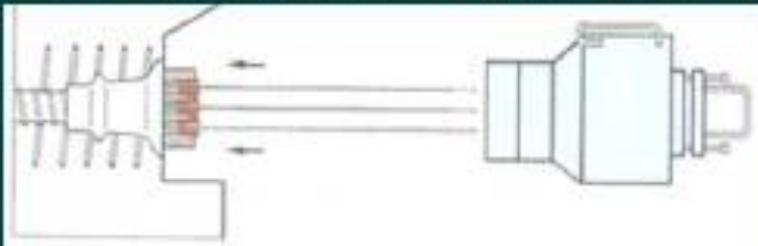
Redoslijed operacija pri zatezaju

Zatezanje kablova može da se vrši sa jednog ili sa oba kraja.

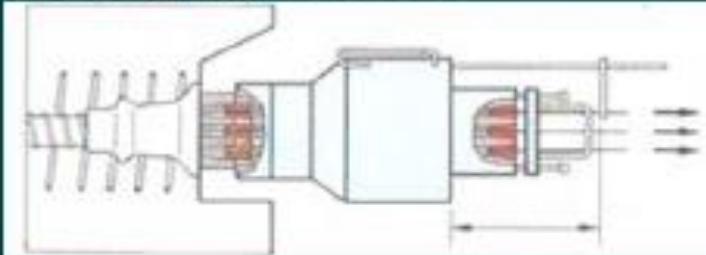
Ukoliko se zateže samo sa jednog kraja na drugom kraju se postavlja fiksna kotva.



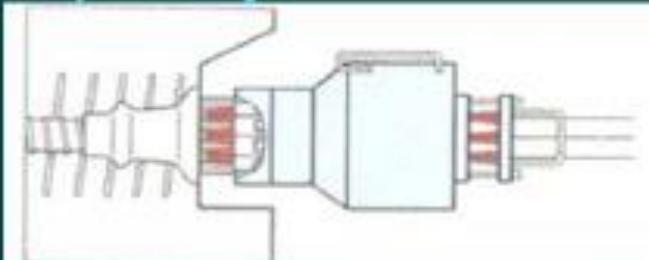
Postavljanje sidrenog bloka i klinova



Postavljanje preše



Naprezanje



Ukljinjavanje



Postavljanje sidrene glave



Postavljanje preše

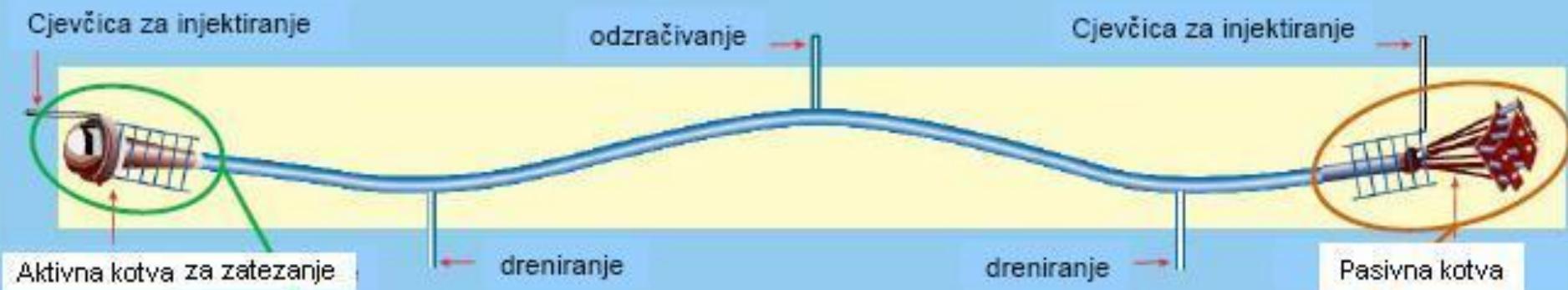


Naprezanje, mjerjenje, ukljinjavanje



Injectiranje

Sidrenje i injektiranje

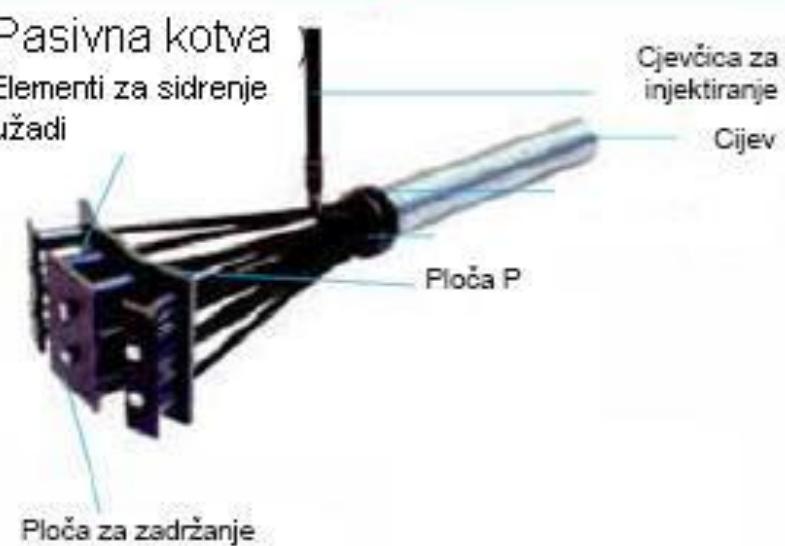


VSL

Aktivna kotva



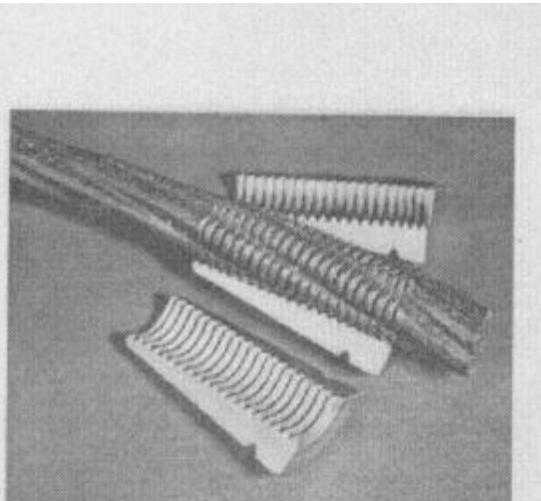
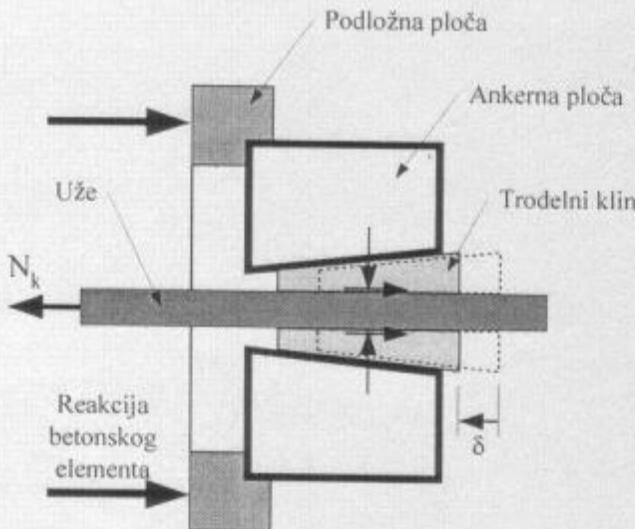
Pasivna kotva
Elementi za sidrenje
užadi



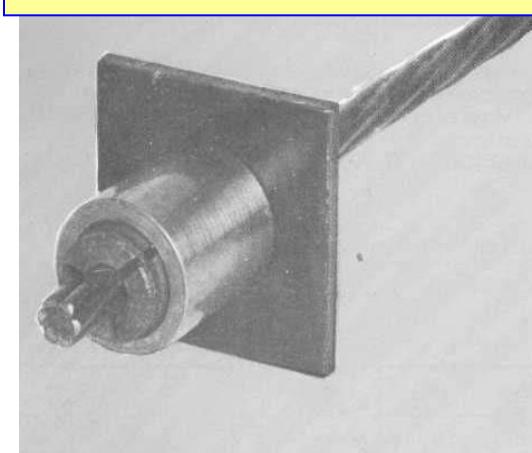
Sidrenje kablova kod naknadnog zatezanja se vrši pomoću:

- Kotve sa klinovima (kod većine sistema)
- Kotve za žice sa glavicama oblikovanim u hladnom stanju (BBR sistem)
- Kotve sa navojima za sidrenje šipki (DYWIDAG sistem)

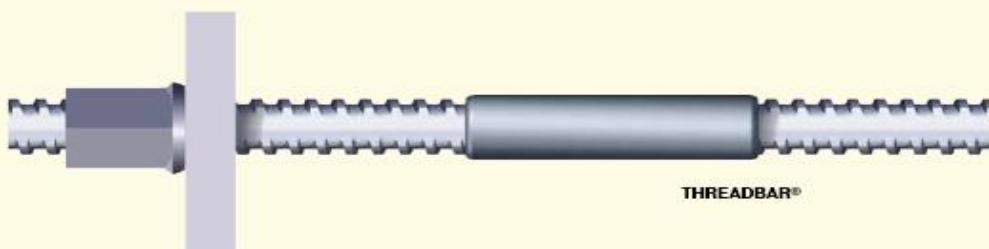
Princip zaklinjavanja



Kotva sa klinom



Sidrenje šipke pomoću navoja i matice



Kotva za žice sa glavicama



Vrste kotvi

- aktivne (normalne, pokretne)
- fiksne (nepokretne)
- nastavne kotve.



Fiksna kotva

Fiksna kotva



Aktivna (normalna)
kotva sa klinovima



Aktivna kotva BBR sistema

Anchorage A
CONA CMI BT
with BBR.VT Plastic Duct

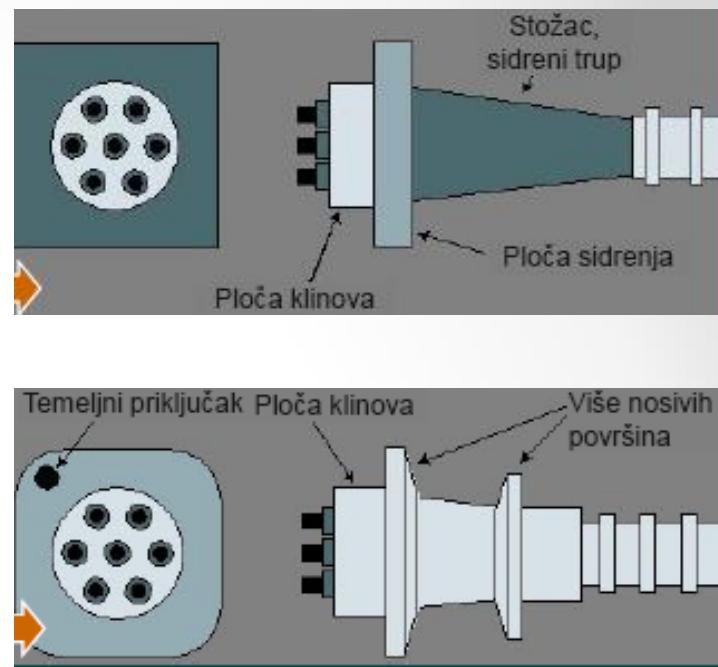


Nastavna kotva BBR sistema

Kablovi savremenih sistema za prethodno naprezanje se sidre pomoću kotve sa klinovima.

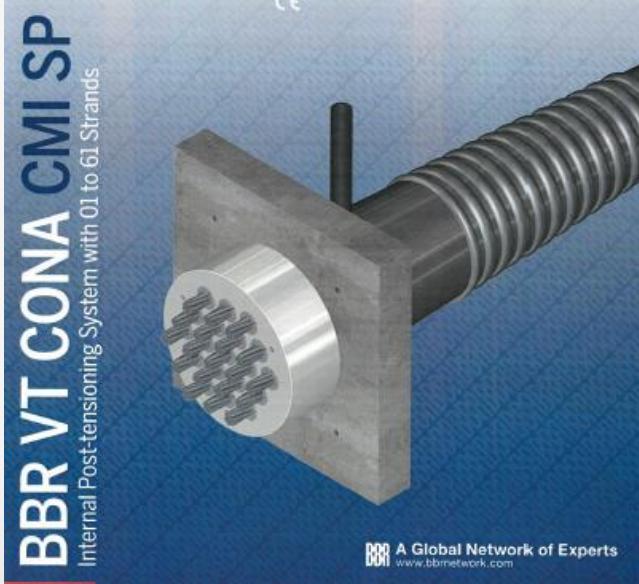
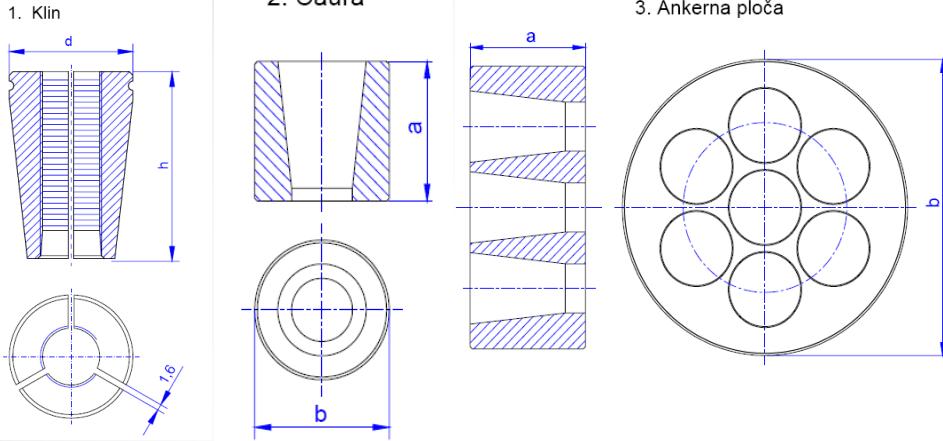
Aktivna kotva se postavlja na mjestu zatezanja kablova. Elementi aktivne kotve:

1. Klin (trodjelni)
2. Čaure (za pojedinačno ukotvljavanje užadi)
3. Ankerne ploče (sa više konusnih otvora)
4. Ravna podložna ploča (square plate)
5. Podložna ploča sa rebrima (bearing trumplate)
6. Konusni nastavak (trumpet)
7. Ravna podložna ploča se koristi za sidrenje u pločastim elementima, dok se za sidrenje većih kablova koriste ploče sa rebrima, koje imaju više površina za prenos sile.

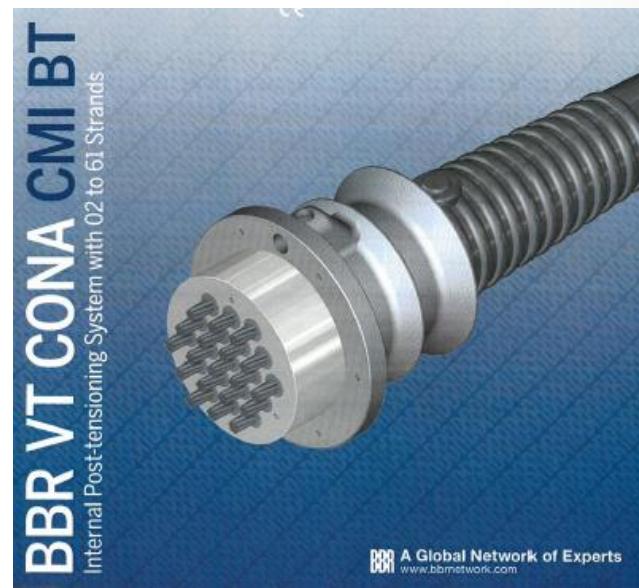
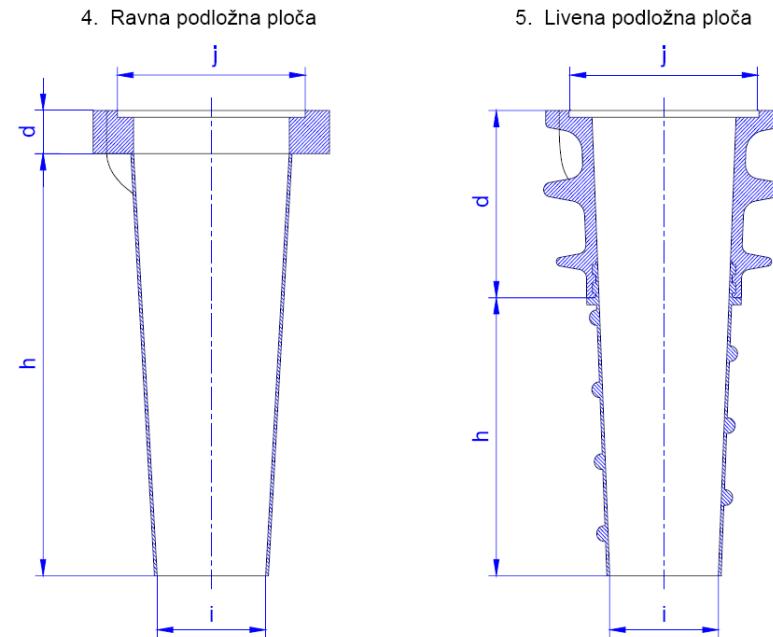


Fiksna (nepokretna) kotva se koristi umjesto normalne kotve u slučajevima kada postoje konstruktivne mogućnosti i kada je jedan kraj nepristupačan za prethodno naprezanje. Konstruktivne mogućnosti podrazumijevaju dovoljnu masu nosača da se kotva može montirati i ako se puna sila prethodnog naprezanja može uvesti na rastojanju " d " od kraja kotve.

Nastavna kotva služi za nastavljanje i produžavanje kablova. Primjenjuje se kod kablova koji nijesu prethodno napregnuti, koji su djelimično prethodno napregnuti kao i kod potpuno prethodno napregnutih kablova. U prva dva slučaja na dužinu " a " koja je data u tablici mora se dodati izduženje kabla koji se nastavlja.



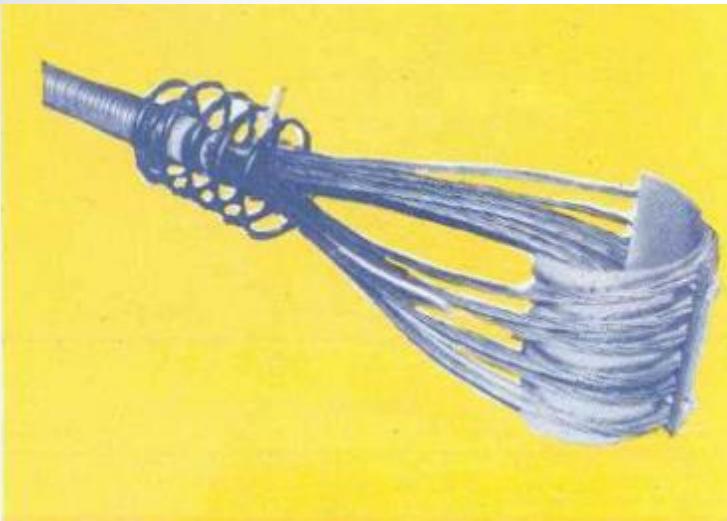
Normalna kotva sa ravnom podložnom pločom



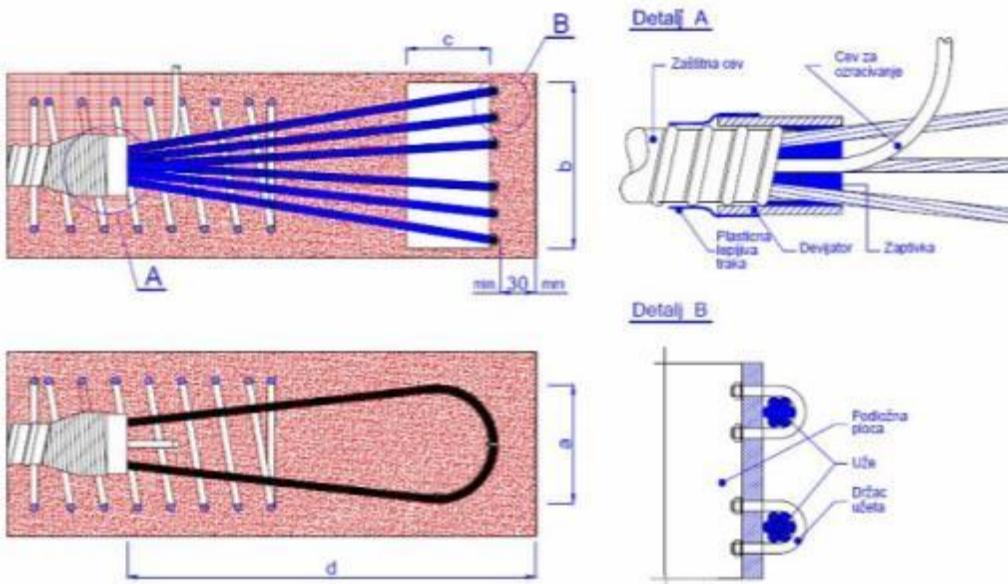
Normalna kotva sa livenom podložnom pločom

Fiksne (nepokretne) kotve

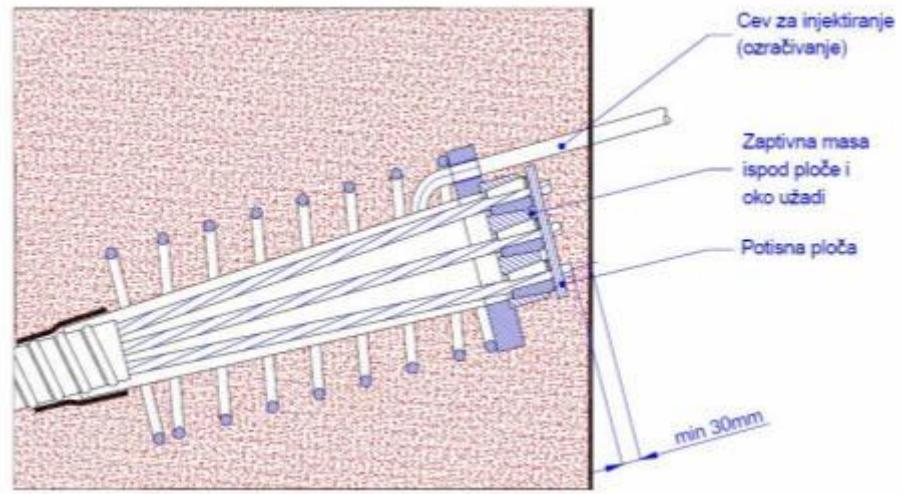
sa previjanjem užadi



1. Skica fiksne kotve sa previjanjem užadi



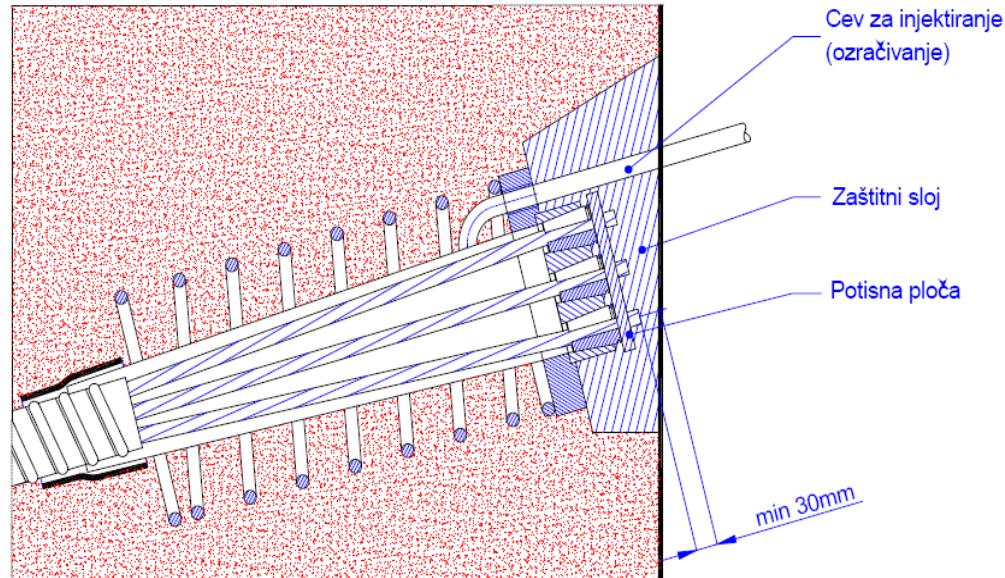
izrađena od normalne kotve



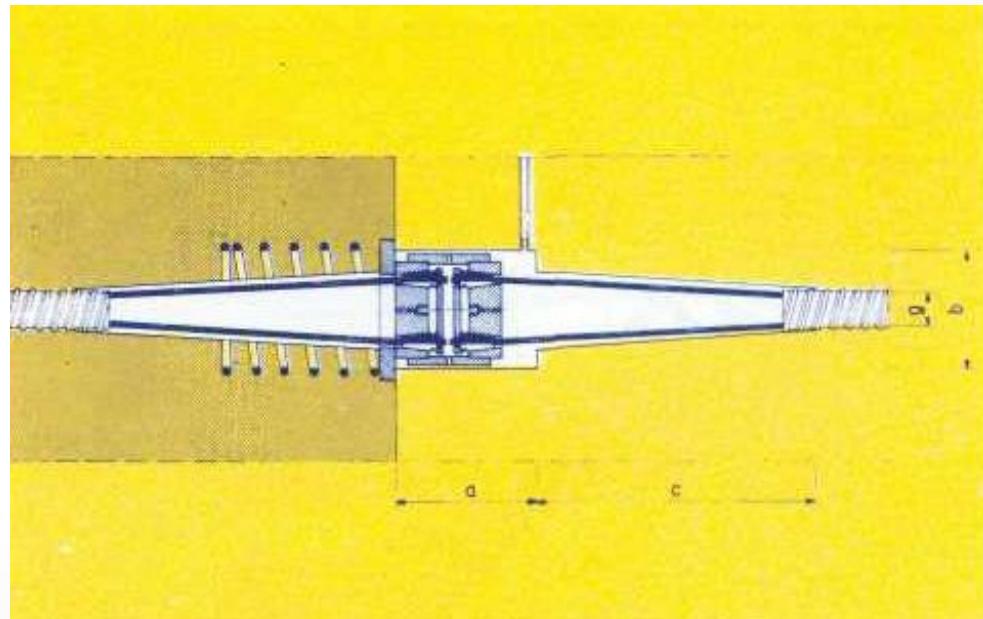
Fiksna kotva izrađena od normalne kotve primjenjuje se kad je konstrukcija nepristupačna sa jedne strane a silu prethodnog naprezanja je neophodno unijeti od samog čela nosača

Pasivna kotva

Pasivna kotva se primjenjuje kad je moguće prethodno naprezanje izvesti samo sa jedne strane i/ili kad je pristup sa jedne strane ograničen. Izrađuje se kao normalna kotva sa skraćenim kablovima.



Nastavljanje kablova



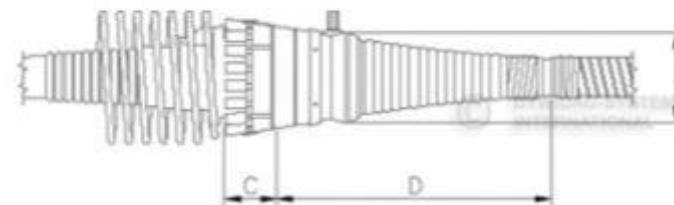
Nastavljanje kablova



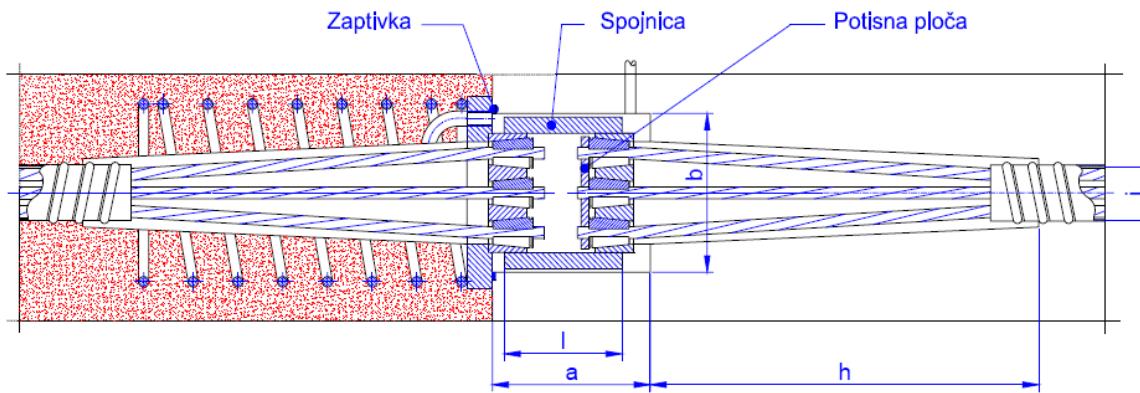
Nastavna kotva BBR
sistema za više užadi



1. Skica nastavne kotve



Nastavna kotva



Nastavna kotva za jedno
uže (monostrand)



Provjera položaja cijevi – rebraste z.c.



Glatke zaštitne cijevi



Podužne i poprečne cijevi



Uvlačenje pojedinačnih kablova





Umetanje klinova



Klinovi u ankernoj ploči



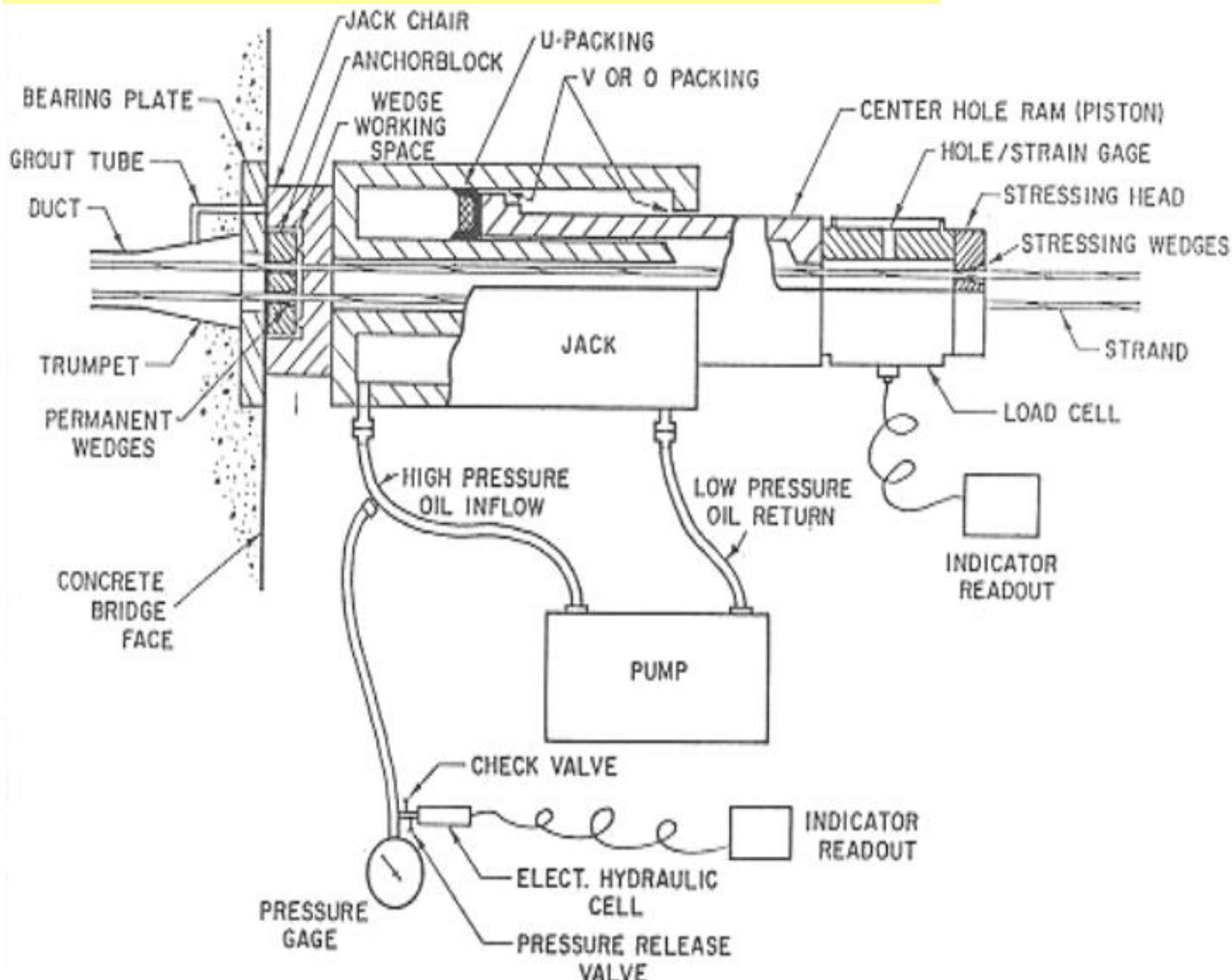
Postavljanje uređaja za sidrenje i prese



Izgled ankernog bloka



Šematski prikaz djelova sistema za naknadno zatezanje



Injektiranje kablova

Oprema za spravljanje i pumpanje injekcione smješte



Mixing and pumping equipment

Odzračivanje



Venting operation

Trajinost konstrukcija sa naknadno zategnutim kablovima sa spojem u velikoj mjeri zavisi od uspješno obavljenog injektiranja.

Očvrsla cementna pasta stvara vezu između zategnutog elementa i betona, obezbjeduje dugotrajnu korozionu zaštitu čelika za prethodno naprezanje.

Priklučenje dovoda injekcione smješte

Sistemi prethodnog naprezanja

BBR sistem

DYWIDAG sistem

VSL sistem

FREYSSINET-ov sistem

MAGNEL-ov sistem

Uvodne napomene

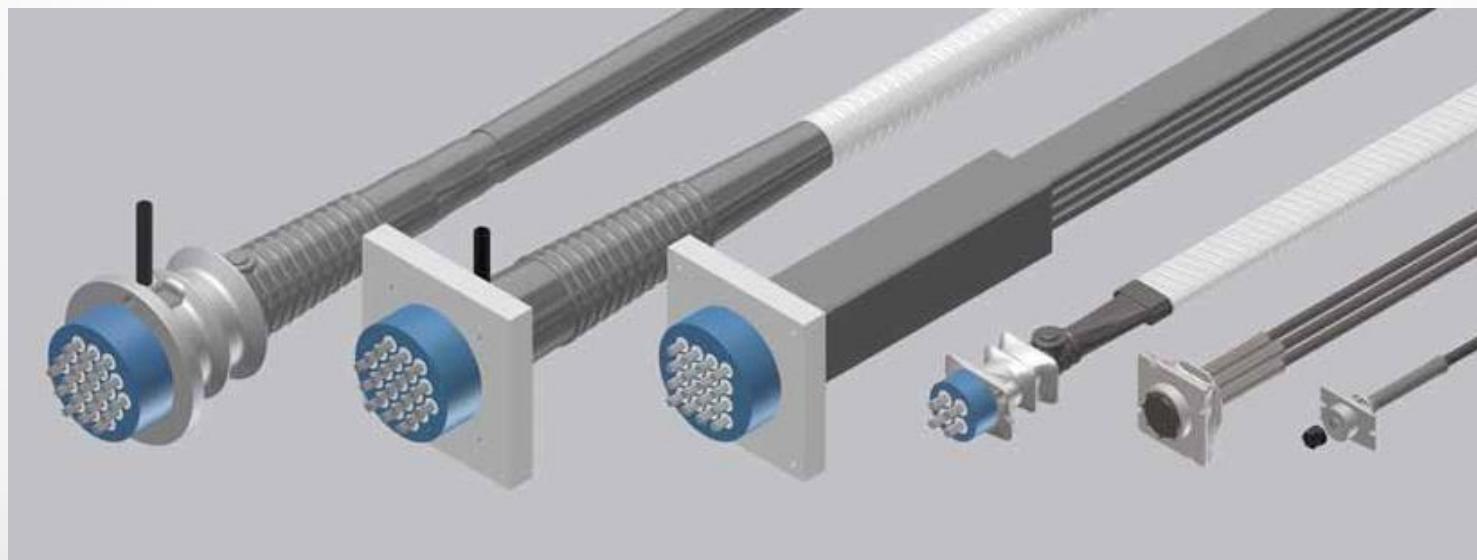
Evropska regulativa 305/2011 i sistemi za prethodno naprezanje

- Uredba za građevinske proizvode / Regulation No. 305/2011 (Construction Products Regulation, or CPR) Evropskog Parlamenta i Evropskog Savjeta (of the European Parliament and of the European Council) je uredba od 9. marta 2011. kojom se utvrđuju usaglašeni uslovi za plasiranje građevinskih proizvoda i zamjenjuje Direktivu (89/106/EEC). Uloga Regulative je da pojasni okvir za stavljanje građevinskih proizvoda na tržište.
- U skladu sa Regulativom primjena sistema prethodnog naprezanja uslovljena je posjedovanjem ETA (European Technical Approval /European Technical Assessment) :

BBR SISTEM

- U okviru mreže BBR je razvijen modularni sistem za naknadno zatezanje BBR VT CONA CMX. Sastoji se od pet glavnih sistema:
- Ovaj sistem se primjenjuju u skladu sa Evropskim Tehničkim Odobrenjem (European Technical Approval).

- ◆ BBR VT CONA CMI – Internal post-tensioning system
- ◆ BBR VT CONA CME – External post-tensioning system
- ◆ BBR VT CONA CMF – Flat anchorage post-tensioning system
- ◆ BBR VT CONA CMM – Monostrand post-tensioning system
- ◆ BBR VT CONA CMB – Band post-tensioning system



Sistem BBR VT CONA

<http://www.bbrnetwork.com/downloads/approvals/etas.html>

BBR VT CONA CMI - internal

BBR VT CONA CMI BT

Internal post-tensioning system

ETA-09/0286: 2 to 61 number strands for internal PT applications with **bearing trumplate** load transfer element.



BBR VT CONA CMI SP

Internal post-tensioning system

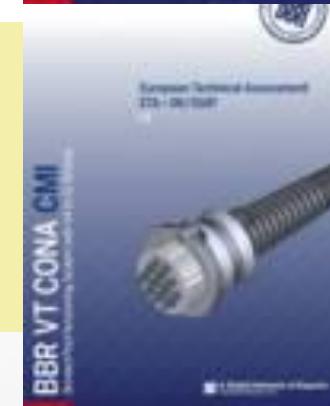
ETA-09/0287: 1 to 61 number strands for internal PT applications with **square plate** load transfer element.



BBR VT CONA CMI –

Internal post-tensioning system

ETA-06/0147: Bonded Post tensioning System with 04 to 31 Strands



BBR VT CONA CME - external

BBR VT CONA CME
External post-tensioning system

ETA-07/0168: 4 to 31 strands for external PT applications.



BBR VT CONA CMF - flat

BBR VT CONA CMF
Internal flat post-tensioning system

ETA-12/0076: 2 to 4 number strands for internal flat PT applications.



BBR VT CONA CMM - monostrand

BBR VT CONA CMM

Monostrand post-tensioning system

ETA-06/0165: 1 to 4 number monostrands
for internal PT applications.



BBR VT CONA CMM Single

Monostrand post-tensioning system

ETA-12/0282: single monostrands for
internal PT applications.



BBR VT CONA CMB - band

BBR VT CONA CMB

Unbonded band post-tensioning system

ETA-10/0065: 1 to 16 number strands for
external band PT applications.



Sistem BBR VT CONA CMI (internal)

- U ovom sistemu koriste se užad od sedam žica.
- Koriste se užad od čelika karakteristične čvrstoće 1860 MPa, kao i 1770 MPa, nominalnog prečnika 15.3 mm, površine poprečnog presjeka 140 mm^2 i 15.7 mm površine poprečnog presjeka 150 mm^2 .
- Kablovi se izrađuju upotrebom od 1 do 61 užeta od po sedam žica (2 do 61 za sistem sa livenom podložnom pločom).
- Karakteristična prekidna sila raspoloživih kablova je od 248 do 17019 kN.

Kablovi sistema BBR sa ravnom podložnom pločom

BBR VT CONA CMI SP – Internal Post-tensioning System with 01 to 61 Strands,

comprising the following components:

- Tendon
 - Internal tendons with 01 to 61 tensile elements.
- Tensile element
 - 7-wire prestressing steel strand with nominal diameter and maximum characteristic tensile strength as given in Table 1.

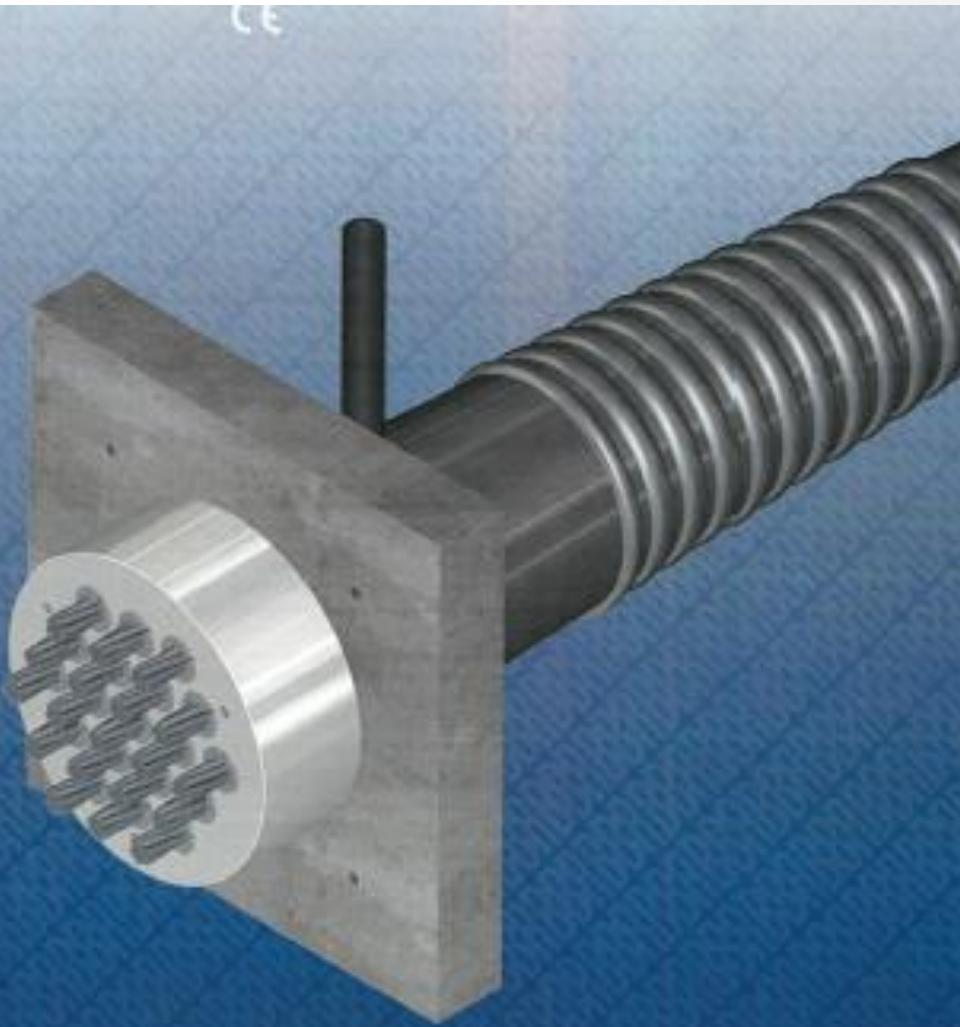
Table 1: Tensile elements

| Nominal diameter | Nominal cross-sectional area | Maximum characteristic tensile strength |
|------------------|------------------------------|---|
| mm | mm ² | MPa |
| 15.3 | 140 | 1 860 |
| 15.7 | 150 | |

NOTE 1 MPa = 1 N/mm²

BBR VTCONA CMI SP

Internal Post-tensioning System with 01 to 61 Strands



BBR A Global Network of Experts
www.bbnetwork.com

Elementi sistema BBR sa livenom podložnom pločom (trumpet bearing)

BBR VT CONA CMI BT – Internal Post-tensioning System with 02 to 61 Strands,

comprising the following components:

- Tendon
 - Internal tendons with 02 to 61 tensile elements.
- Tensile element
 - 7-wire prestressing steel strand with nominal diameter and maximum characteristic tensile strength as given in Table 1.

Table 1: Tensile elements

| Nominal diameter | Nominal cross-sectional area | Maximum characteristic tensile strength |
|------------------|------------------------------|---|
| mm | mm ² | MPa |
| 15.3 | 140 | 1 860 |
| 15.7 | 150 | |

NOTE 1 MPa = 1 N/mm²

BBR VTCONA CMI BT

Internal Post-tensioning System with 02 to 61 Strands



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www.bbrnetwork.com

Elementi sistema BBR sa livenom podložnom pločom

- Anchorage and coupler

Anchorage of the strands with ring wedges;

End anchorage

Fixed (passive) anchor or stressing (active) anchor as end anchorage for 02, 03, 04, 05, 06, 07, 08, 09, 12, 13, 15, 16, 19, 22, 24, 25, 27, 31, 37, 42, 43, 48, 55 and 61 strands;

Fixed or stressing coupler

Single plane coupler for 02, 03, 04, 05, 06, 07, 08, 09, 12, 13, 15, 16, 19, 22, 24, 25, 27, and 31 strands;

Sleeve coupler for 02, 03, 04, 05, 06, 07, 08, 09, 12, 13, 15, 16, 19, 22, 24, 25, 27, 31, 37, 42, 43, 48, 55 and 61 strands;

Movable coupler

Single plane coupler for 02, 03, 04, 05, 06, 07, 08, 09, 12, 13, 15, 16, 19, 22, 24, 25, 27, and 31 strands;

Sleeve coupler for 02, 03, 04, 05, 06, 07, 08, 09, 12, 13, 15, 16, 19, 22, 24, 25, 27, 31, 37, 42, 43, 48, 55 and 61 strands;

- Bearing trumplate for 02, 03, 04, 05, 06, 07, 08, 09, 12, 13, 15, 16, 19, 22, 24, 25, 27, 31, 37, 42, 43, 48, 55 and 61 strands;
- Helix and additional reinforcement in the region of the anchorage;
- Corrosion protection for tensile elements, couplers and anchorages.

| Number of strands | Nominal cross-sectional area of prestressing steel | Nominal mass of prestressing steel | Characteristic value of maximum force of tendon | |
|-------------------|--|------------------------------------|---|-------------------------------|
| | | | $f_{pk} = 1\ 770 \text{ MPa}$ | $f_{pk} = 1\ 860 \text{ MPa}$ |
| n | A_p | M | F_{pk} | F_{pk} |
| — | mm ² | kg/m | kN | kN |
| 02 | 280 | 2.2 | 496 | 520 |
| 03 | 420 | 3.3 | 744 | 780 |
| 04 | 560 | 4.4 | 992 | 1 040 |
| 05 | 700 | 5.5 | 1 240 | 1 300 |
| 06 | 840 | 6.6 | 1 488 | 1 560 |
| 07 | 980 | 7.7 | 1 736 | 1 820 |
| 08 | 1 120 | 8.7 | 1 984 | 2 080 |
| 09 | 1 260 | 9.8 | 2 232 | 2 340 |
| 12 | 1 680 | 13.1 | 2 976 | 3 120 |
| 13 | 1 820 | 14.2 | 3 224 | 3 380 |
| 15 | 2 100 | 16.4 | 3 720 | 3 900 |
| 16 | 2 240 | 17.5 | 3 968 | 4 160 |
| 19 | 2 660 | 20.8 | 4 712 | 4 940 |
| 22 | 3 080 | 24.0 | 5 456 | 5 720 |
| 24 | 3 360 | 26.2 | 5 952 | 6 240 |
| 25 | 3 500 | 27.3 | 6 200 | 6 500 |
| 27 | 3 780 | 29.5 | 6 696 | 7 020 |
| 31 | 4 340 | 33.9 | 7 688 | 8 060 |
| 37 | 5 180 | 40.4 | 9 176 | 9 620 |
| 42 | 5 880 | 45.9 | 10 416 | 10 920 |
| 43 | 6 020 | 47.0 | 10 664 | 11 180 |
| 48 | 6 720 | 52.5 | 11 904 | 12 480 |
| 55 | 7 700 | 60.1 | 13 640 | 14 300 |
| 61 | 8 540 | 66.7 | 15 128 | 15 860 |

Kablovi sistema

BBR VT
Cona CMI BT

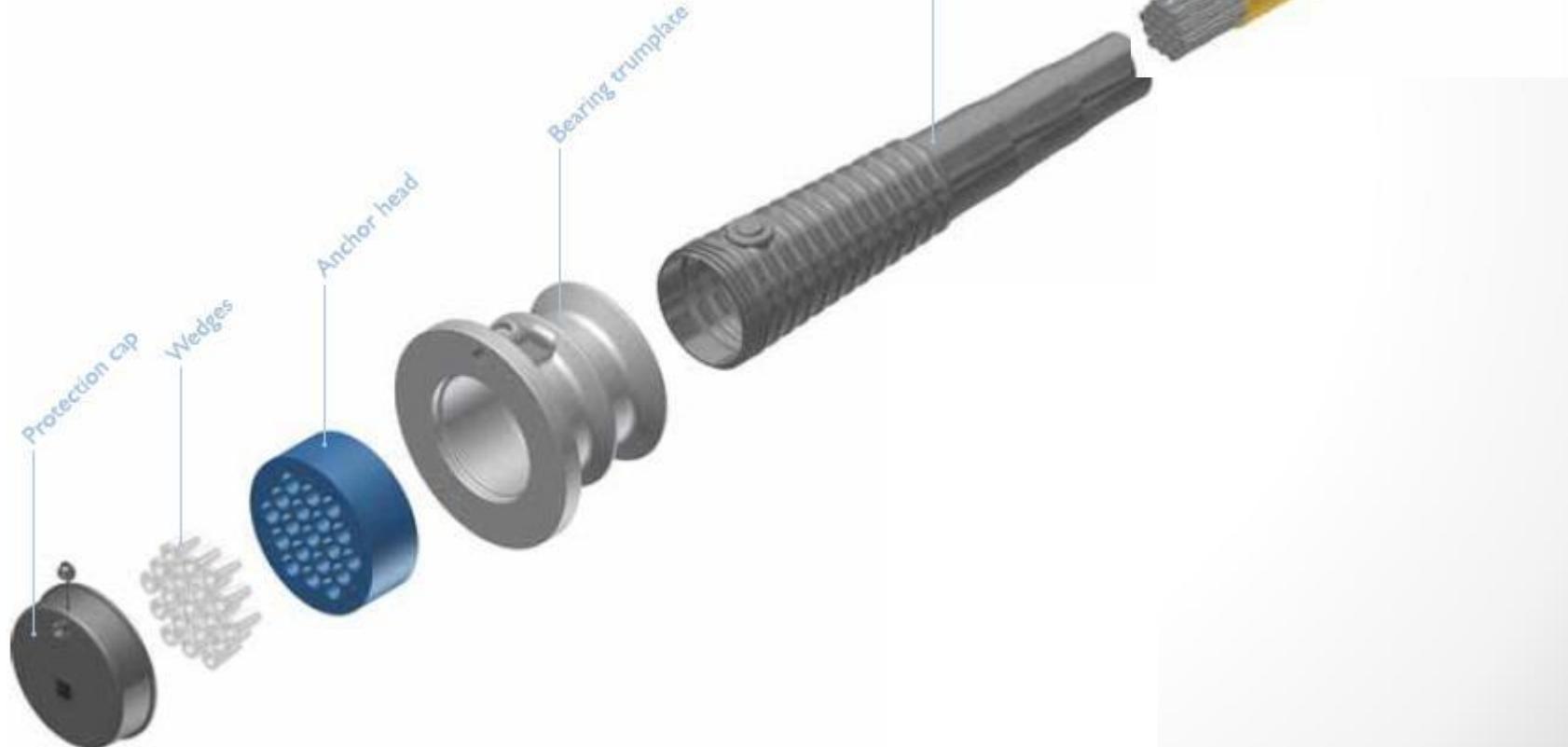
| Number of strands | Nominal cross-sectional area of prestressing steel | Nominal mass of prestressing steel | Characteristic value of maximum force of tendon | |
|-------------------|--|------------------------------------|---|-------------------------------|
| | | | $f_{pk} = 1\ 770 \text{ MPa}$ | $f_{pk} = 1\ 860 \text{ MPa}$ |
| n | A_p | M | F_{pk} | F_{pk} |
| — | mm^2 | kg/m | kN | kN |
| 02 | 300 | 2.3 | 532 | 558 |
| 03 | 450 | 3.5 | 798 | 837 |
| 04 | 600 | 4.7 | 1 064 | 1 116 |
| 05 | 750 | 5.9 | 1 330 | 1 395 |
| 06 | 900 | 7.0 | 1 596 | 1 674 |
| 07 | 1 050 | 8.2 | 1 862 | 1 953 |
| 08 | 1 200 | 9.4 | 2 128 | 2 232 |
| 09 | 1 350 | 10.5 | 2 394 | 2 511 |
| 12 | 1 800 | 14.1 | 3 192 | 3 348 |
| 13 | 1 950 | 15.2 | 3 458 | 3 627 |
| 15 | 2 250 | 17.6 | 3 990 | 4 185 |
| 16 | 2 400 | 18.8 | 4 256 | 4 464 |
| 19 | 2 850 | 22.3 | 5 054 | 5 301 |
| 22 | 3 300 | 25.8 | 5 852 | 6 138 |
| 24 | 3 600 | 28.1 | 6 384 | 6 696 |
| 25 | 3 750 | 29.3 | 6 650 | 6 975 |
| 27 | 4 050 | 31.6 | 7 182 | 7 533 |
| 31 | 4 650 | 36.3 | 8 246 | 8 649 |
| 37 | 5 550 | 43.4 | 9 842 | 10 323 |
| 42 | 6 300 | 49.2 | 11 172 | 11 718 |
| 43 | 6 450 | 50.4 | 11 438 | 11 997 |
| 48 | 7 200 | 56.3 | 12 768 | 13 392 |
| 55 | 8 250 | 64.5 | 14 630 | 15 345 |
| 61 | 9 150 | 71.5 | 16 226 | 17 019 |

**Kablovi sistema
BBR**
**BBR VT Cona
CMI BT**

Komponente kablova sa ankernim dijelom za naknadno zatezanje

BBR VT CONA CMI

internal post tensioning system

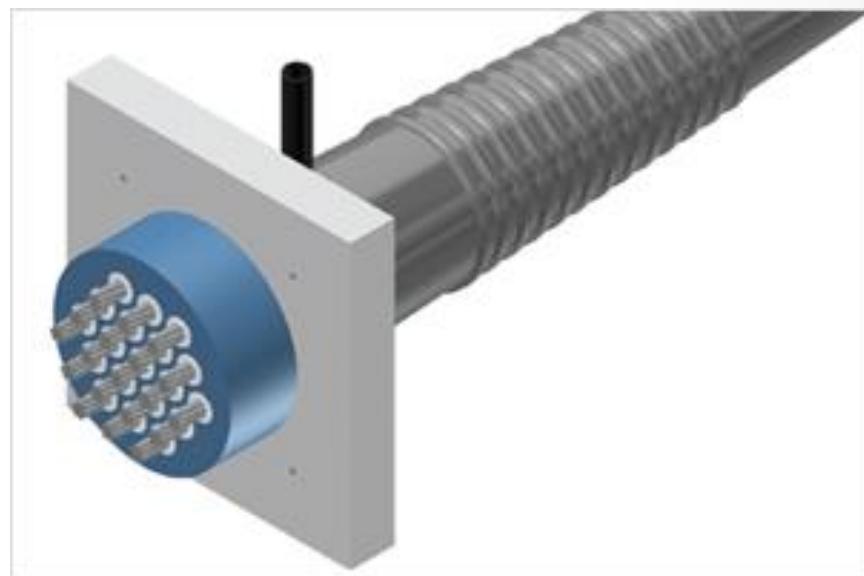


BBR VT CONA CME external post-tensioning system

The European approved CONA® CME post-tensioning system is the ultimate multi-strand technology for all types of externally post-tensioned applications. The standard tendon sizes range from 1 to 73 strands. CONA CME can be applied for the prestressing of bridges, precast segmental construction and repair and strengthening works of all kind of structures.



CONA CME BT



CONA CME SP

VSL Sistem

Internal tendons – the most commonly-used solution

The VSL systems are based on the method of post-tensioning. Most applications of the multi-strand system are internal and cement grouted, providing bond to the structure. Such tendons are extensively used in bridges and transportation structures as well as being applied successfully in building construction.

Shenzhen Western Corridor,
Hong Kong - 2004



1 - STRAND

1.1 - STRAND PROPERTIES 13mm (0.5")

| Strand type | prEN 10138 – 3 (2006) Y1860S7 | | | ASTM A 416-06 Grade 270 |
|---|--------------------------------------|-------------------|-------------------|----------------------------|
| Nominal diameter | d (mm) | 12.5 | 12.9 | 12.7 |
| Nominal cross section | A _p (mm ²) | 93 | 100 | 98.7 |
| Nominal mass | M (kg/m) | 0.726 | 0.781 | 0.775 |
| Nominal yield strength | f _{p0,1k} (MPa) | 1634 ¹ | 1640 ¹ | 1675 ² |
| Nominal tensile strength | f _{pk} (MPa) | 1860 | 1860 | 1860 |
| Specif./min. breaking load | F _{pk} (kN) | 173 | 186 | 183.7 |
| Young's modulus | (GPa) | | approx. 195 | |
| Relaxation ³ after 1000 h at 20°C and 0.7 x F _{pk} | (%) | | max. 2.5 | |

1) Characteristic value measured at 0.1% permanent extension

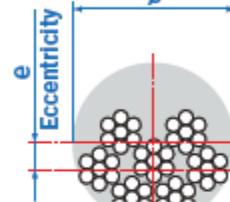
2) Minimum load at 1% extension for low-relaxation strand

3) Valid for relaxation class acc. to prEN 10138-3 or low-relaxation grade acc. to ASTM A 416-06

1.2 - TENDON PROPERTIES 13mm (0.5")

| Unit | Strands numbers | Steel area | | | Breaking load | | | Corrugated steel duct ³ (recommended) | Corrugated plastic duct VSL PT-PLUS® | | |
|------|-----------------|---|--|--|---|--|---|---|---|--------------------|----|
| | | A _p acc. to prEN | | ASTM | Y1860S7 (prEN) | | Grade 270 (ASTM) | | | | |
| | | d=12.5 mm A _p =93 mm ² | d=12.9 mm A _p =100 mm ² | d=12.7 mm A _p =100 mm ² | d=12.5 mm A _p =93 mm ² | d=12.9 mm A _p =100 mm ² | d=12.7 mm A _p =98.7 mm ² | | | | |
| | | [mm ²] | [mm ²] | [mm ²] | [kN] | [kN] | [kN] | [mm] | [mm] | [mm] | |
| 5-1 | 1 | 93 | 100 | 98.7 | 173 | 186 | 183.7 | 20/25 | 3 | 22/25 | 6 |
| 5-2 | 2 | 186 | 200 | 197 | 346 | 372 | 367 | 35/40 | 8 | 76/25 ² | - |
| 5-3 | 3 | 279 | 300 | 296 | 519 | 558 | 551 | 35/40 | 6 | 76/25 ² | - |
| 5-4 | 4 | 372 | 400 | 395 | 692 | 744 | 735 | 40/45 ¹ | 7 | 76/25 ² | - |
| 5-7 | 5 | 465 | 500 | 494 | 865 | 930 | 919 | 45/50 | 8 | 58/63 | 14 |
| | 6 | 558 | 600 | 592 | 1038 | 1116 | 1102 | 45/50 | 6 | 58/63 | 12 |
| 5-7 | 7 | 651 | 700 | 691 | 1211 | 1302 | 1286 | 50/57 | 7 | 58/63 | 11 |
| 5-12 | 8 | 744 | 800 | 790 | 1384 | 1488 | 1470 | 55/62 | 9 | 58/63 | 10 |
| | 9 | 837 | 900 | 888 | 1557 | 1674 | 1653 | 55/62 | 8 | 58/63 | 9 |
| | 10 | 930 | 1000 | 987 | 1730 | 1860 | 1837 | 60/67 | 10 | 58/63 | 9 |
| | 11 | 1023 | 1100 | 1086 | 1903 | 2046 | 2021 | 60/67 | 9 | 58/63 | 8 |
| 5-12 | 12 | 1116 | 1200 | 1184 | 2076 | 2232 | 2204 | 60/67 | 8 | 58/63 | 7 |
| 5-15 | 13 | 1209 | 1300 | 1283 | 2249 | 2418 | 2388 | 65/72 | 9 | 76/81 | 14 |
| | 14 | 1302 | 1400 | 1382 | 2422 | 2604 | 2572 | 65/72 | 8 | 76/81 | 13 |
| 5-15 | 15 | 1395 | 1500 | 1481 | 2595 | 2790 | 2756 | 70/77 | 9 | 76/81 | 12 |
| 5-19 | 16 | 1488 | 1600 | 1579 | 2768 | 2976 | 2939 | 70/77 | 9 | 76/81 | 12 |
| | 17 | 1581 | 1700 | 1678 | 2941 | 3162 | 3123 | 75/82 | 11 | 76/81 | 11 |
| | 18 | 1674 | 1800 | 1777 | 3114 | 3348 | 3307 | 75/82 | 10 | 76/81 | 10 |
| 5-19 | 19 | 1767 | 1900 | 1875 | 3287 | 3534 | 3490 | 75/82 | 9 | 76/81 | 9 |
| 5-22 | 20 | 1860 | 2000 | 1974 | 3460 | 3720 | 3674 | 80/87 | 10 | 100/106 | 20 |

Prikazan je dio tabele. Najveći kablovi sadrže 55 užadi i zatežu se max silom pri prekidu 10230 kN.



1.3 - STRAND PROPERTIES 15mm (0.6")

| Strand type | prEN 10138 – 3 (2006) Y1860S7 | | | ASTM A 416-06 Grade 270 |
|---|--------------------------------------|-------------------|-------------------|----------------------------|
| Nominal diameter | d (mm) | 15.3 | 15.7 | 15.24 |
| Nominal cross section | A _p (mm ²) | 140 | 150 | 140 |
| Nominal mass | M (kg/m) | 1.093 | 1.172 | 1.102 |
| Nominal yield strength | f _{p0,1k} (MPa) | 1636 ¹ | 1640 ¹ | 1676 ² |
| Nominal tensile strength | f _{pk} (MPa) | 1860 | 1860 | 1860 |
| Specif./min. breaking load | F _{pk} (kN) | 260 | 279 | 260.7 |
| Young's modulus | (GPa) | | approx. 195 | |
| Relaxation ³ after 1000 h at 20°C and 0.7 x F _{pk} | (%) | | max. 2.5 | |

1) Characteristic value measured at 0.1% permanent extension

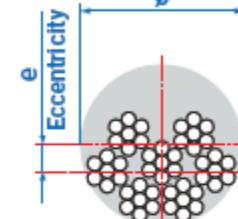
2) Minimum load at 1% extension for low-relaxation strand

3) Valid for relaxation class acc. to prEN 10138-3 or low-relaxation grade acc. to ASTM A 416-06

1.4 - TENDON PROPERTIES 15mm (0.6")

| Unit | Strands numbers | Steel area | | | Breaking load | | | Corrugated steel duct ³ (recommended) | Corrugated plastic duct VSL PT-PLUS® | | |
|------|-----------------|-------------------------------------|-------------------------------------|--------------------------------------|-------------------------------------|-------------------------------------|--------------------------------------|---|---|--------------------|----|
| | | Ap acc. to prEN | | ASTM | Y1860S7 (prEN) | | Grade 270 (ASTM) | | | | |
| | | d=15.3 mm Ap=140 mm ² | d=15.7 mm Ap=150 mm ² | d=15.24 mm Ap=140 mm ² | d=15.3 mm Ap=140 mm ² | d=15.7 mm Ap=150 mm ² | d=15.24 mm Ap=140 mm ² | [mm] | [kN] | [mm] | |
| 6-1 | 1 | 140 | 150 | 140 | 260 | 279 | 260.7 | 25/30 | 5 | 22/25 | 4 |
| 6-2 | 2 | 280 | 300 | 280 | 520 | 558 | 521 | 40/45 | 9 | 76/25 ² | - |
| 6-3 | 3 | 420 | 450 | 420 | 780 | 837 | 782 | 40/45 | 6 | 76/25 ² | - |
| 6-4 | 4 | 560 | 600 | 560 | 1040 | 1116 | 1043 | 45/50 ¹ | 7 | 76/25 ² | - |
| 6-7 | 5 | 700 | 750 | 700 | 1300 | 1395 | 1304 | 50/57 | 8 | 58/63 | 13 |
| | 6 | 840 | 900 | 840 | 1560 | 1674 | 1564 | 55/62 | 9 | 58/63 | 11 |
| 6-7 | 7 | 980 | 1050 | 980 | 1820 | 1953 | 1825 | 55/62 | 7 | 58/63 | 9 |
| 6-12 | 8 | 1120 | 1200 | 1120 | 2080 | 2232 | 2086 | 65/72 | 11 | 76/81 | 18 |
| | 9 | 1260 | 1350 | 1260 | 2340 | 2511 | 2346 | 65/72 | 9 | 76/81 | 16 |
| | 10 | 1400 | 1500 | 1400 | 2600 | 2790 | 2607 | 70/77 | 11 | 76/81 | 15 |
| | 11 | 1540 | 1650 | 1540 | 2860 | 3069 | 2868 | 70/77 | 9 | 76/81 | 13 |
| 6-12 | 12 | 1680 | 1800 | 1680 | 3120 | 3348 | 3128 | 75/82 | 11 | 76/81 | 12 |
| 6-15 | 13 | 1820 | 1950 | 1820 | 3380 | 3627 | 3389 | 80/87 | 13 | 100/106 | 25 |
| | 14 | 1960 | 2100 | 1960 | 3640 | 3906 | 3650 | 80/87 | 11 | 100/106 | 24 |
| 6-15 | 15 | 2100 | 2250 | 2100 | 3900 | 4185 | 3911 | 80/87 | 10 | 100/106 | 23 |
| 6-19 | 16 | 2240 | 2400 | 2240 | 4160 | 4464 | 4171 | 85/92 | 12 | 100/106 | 22 |
| | 17 | 2380 | 2550 | 2380 | 4420 | 4743 | 4432 | 85/92 | 11 | 100/106 | 20 |
| | 18 | 2520 | 2700 | 2520 | 4680 | 5022 | 4693 | 90/97 | 13 | 100/106 | 19 |
| 6-19 | 19 | 2660 | 2850 | 2660 | 4940 | 5301 | 4953 | 90/97 | 12 | 100/106 | 18 |
| 6-22 | 20 | 2800 | 3000 | 2800 | 5200 | 5580 | 5214 | 100/107 | 17 | 100/106 | 17 |
| | 21 | 2940 | 3150 | 2940 | 5420 | 5750 | 5475 | 100/107 | 16 | 100/106 | 16 |

Samo dio tabele je prikazan. Najveći kablovi su sa 55 užadi i silom 15345 kN.



VSLab® S system

This European Technical Approval (ETA) applies to the following post-tensioning kit: VSLab® S system with 2, 3, 4 and 5 strands

Uslov iz Standarda EN 10138-3

$P_{\max} = \min \{k_1 \cdot A_p \cdot f_{pk}; k_2 \cdot A_p \cdot f_{p0.1k}\}$, with $k_1 = 0.8$, $k_2 = 0.9$, $f_{pk} = 1\ 860\ N/mm^2$, $f_{p0.1k} = 0.88\ f_{pk}$

| Qty. of strands | Strand Ø 15.3 $f_{pk} = 1\ 860\ N/mm^2$ | | | | | Strand Ø 15.7 $f_{pk} = 1\ 860\ N/mm^2$ | | | | |
|-----------------|--|--------------------|---------------------------|-----------------------|------------------------------|--|--------------------|---------------------------|-----------------------|------------------------------|
| | A_p | $A_p \cdot f_{pk}$ | 0.8 $A_p \cdot f_{pk}$ | $A_p \cdot f_{p0.1k}$ | 0.9 $A_p \cdot f_{p0.1k}$ | A_p | $A_p \cdot f_{pk}$ | 0.8 $A_p \cdot f_{pk}$ | $A_p \cdot f_{p0.1k}$ | 0.9 $A_p \cdot f_{p0.1k}$ |
| | mm^2 | kN | kN | kN | kN | mm^2 | kN | kN | kN | kN |
| 2 | 280 | 521 | 417 | 459 | 413 | 300 | 558 | 446 | 492 | 443 |
| 3 | 420 | 781 | 625 | 688 | 619 | 450 | 837 | 670 | 738 | 664 |
| 4 | 560 | 1042 | 833 | 917 | 826 | 600 | 1116 | 893 | 984 | 886 |
| 5 | 700 | 1302 | 1042 | 1147 | 1032 | 750 | 1395 | 1116 | 1230 | 1107 |

Note : prestressing force applied to structure must be in accordance with national regulations.

| Qty. of strands | Strand Ø 15.7 $f_{pk} = 1\ 770\ N/mm^2$ $F_{pk} = 265\ kN$ $F_{p0.1k} = 236\ kN$ | | | | |
|--|--|--------------------|---------------------------|-----------------------|------------------------------|
| | A_p | $A_p \cdot f_{pk}$ | 0.8 $A_p \cdot f_{pk}$ | $A_p \cdot f_{p0.1k}$ | 0.9 $A_p \cdot f_{p0.1k}$ |
| | mm^2 | kN | kN | kN | kN |
| 2 | 300 | 530 | 424 | 472 | 425 |
| 3 | 450 | 795 | 636 | 708 | 637 |
| 4 | 600 | 1060 | 848 | 944 | 850 |
| 5 | 750 | 1325 | 1060 | 1180 | 1062 |
| Note : prestressing force applied to structure must be in accordance with national regulations | | | | | |

DYWIDAG sistem

Podaci o užadima

► Technical Data

| type code/specification | | 13 mm (0.5") | | 15 mm (0.6") | | | |
|--|-------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|
| | | ASTM A 416 | prEN 10138 | ASTM A 416 | prEN 10138 | ASTM A 416 | prEN 10138 |
| | | Grade 270 | BS 5896 | Grade 250 | BS 5896 | Grade 270 | BS 5896 |
| yield strength $f_{p0.1k}$ | N/mm ² | 1,670 ¹⁾ | 1,640 ²⁾ | 1,550 ¹⁾ | 1,560 ²⁾ | 1,670 ¹⁾ | 1,640 ²⁾ |
| ultimate strength f_{pk} | N/mm ² | 1,860 | 1,860 | 1,725 | 1,770 | 1,860 | 1,860 |
| nom. diameter | mm | 12.70 | 12.90 | 15.20 | 15.70 | 15.24 | 15.70 |
| cross-sectional area | mm ² | 98.71 | 100.00 | 139.40 | 150.00 | 140.00 | 150.00 |
| weight | kg/m | 0.775 | 0.785 | 1.094 | 1.180 | 1.102 | 1.18 |
| ultimate load | kN | 183.7 | 186.0 | 240.2 | 265.5 | 260.7 | 279.0 |
| modulus of elasticity | N/mm ² | | | ~195,000 | | | |
| relaxation ³⁾ after 1,000 h at 0.7 x ultimate strength f_{pk} | % | | | max. 2.5 | | | |

¹⁾ yield measured at 1% effective elongation

²⁾ yield measured at 0.1% residual elongation

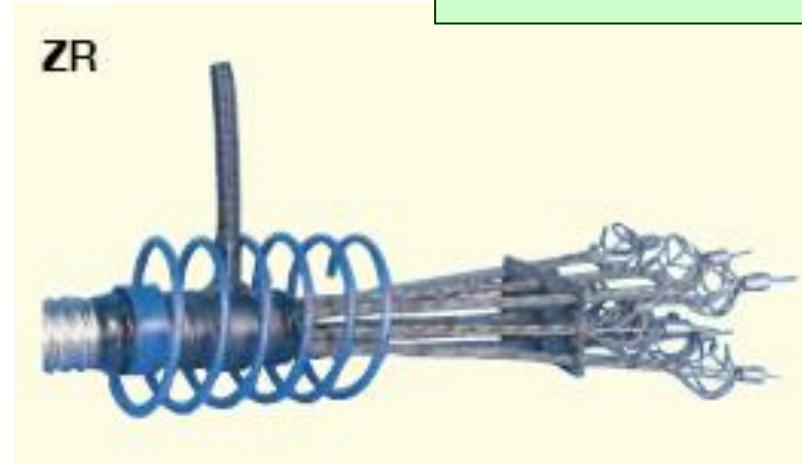
³⁾ applicable for relaxation class 2 according to Eurocode prEN 10138/BS 5896: or low relaxation complying with ASTM A 416, respectively.

DYWIDAG sistem

Aktivna kotva



Fiksna kotva



Kotva za sidrenje
kablova u ploči



DYWIDAG sistem



Prethodno naprezanje ploča



Element za povezivanje užadi kod kružnog prethodnog naprezanja (rezervoara, cijevi velikog prečnika, kupola)



DYWIDAG sistem

Tehnički podaci o šipkama

Technical data

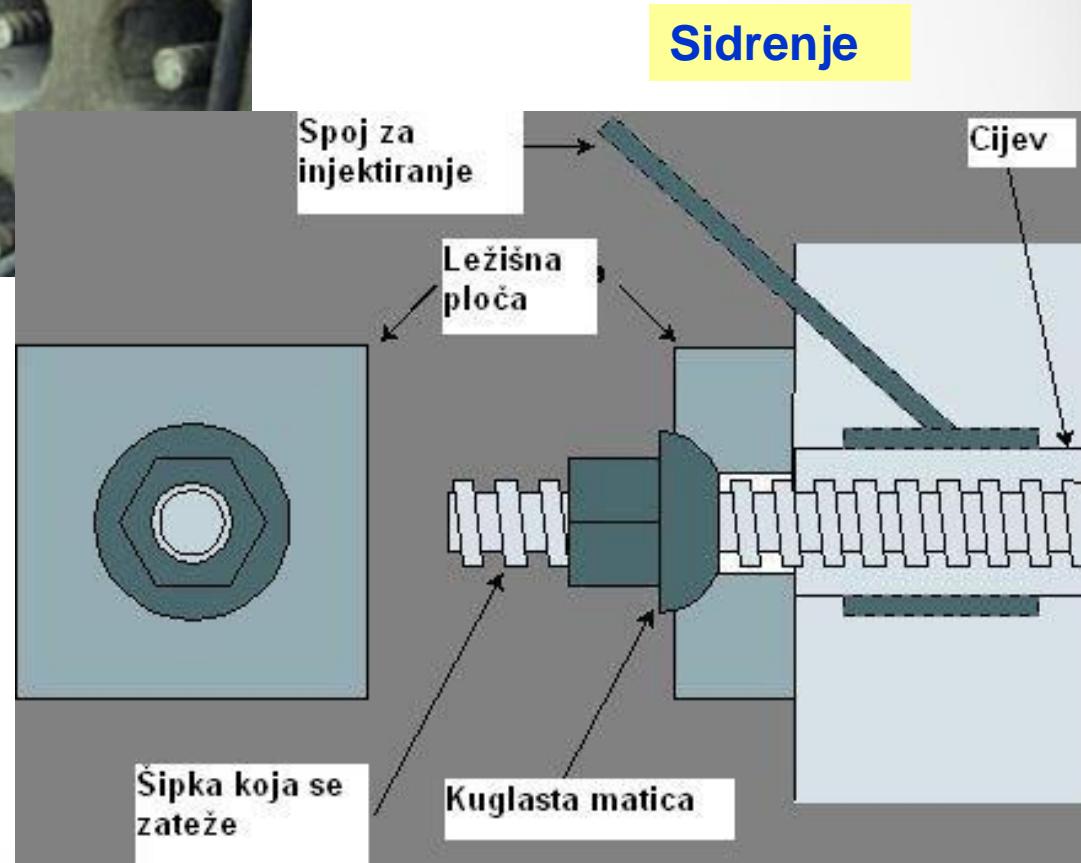
| | THREADBAR® | | | | | | | Plain bar | |
|---|------------|-----------------|--------------------|--------------------|--------------------|---------------------|---------------------|-----------|-------|
| Designation | - | - | 26 WR | 32 WR | 36 WR | 40 WR | 47 WR | 32 WS | 36 WS |
| Nominal diameter | d_n | mm | 26.5 | 32 | 36 | 40 | 47 | 32 | 36 |
| Cross section area | S_n | mm ² | 552 | 804 | 1018 | 1257 | 1735 | 804 | 1018 |
| Nominal mass per metre | M | kg/m | 4.48 ¹⁾ | 6.53 ¹⁾ | 8.27 ¹⁾ | 10.21 ¹⁾ | 14.10 ¹⁾ | 6.31 | 7.99 |
| Pitch | c | mm | 13 | 16 | 18 | 20 | 21 | 3.0 | 3.0 |
| Characteristic breaking load | F_m | KN | 580 | 845 | 1070 | 1320 | 1820 | 845 | 1070 |
| Max. initial stressing force $P_{m0,max} = S_n \times 0.8 \times f_{p0,k}$ | | KN | 464 | 676 | 856 | 1056 | 1456 | 676 | 856 |
| Max. overstressing force $P_{0,max} = S_n \times 0.95 \times f_{p0,k}$ | | KN | 499 | 722 | 912 | 1130 | 1567 | 722 | 912 |

1) The nominal mass per metre includes 3.5% not load bearing portion of ribs.

DYWIDAG sistem



Zatezanje



Sidrenje

DYWIDAG sistem



Uredaj za potiskivanje kablova pri uvlačenju u zaštitne cijevi.



Strand Pusher

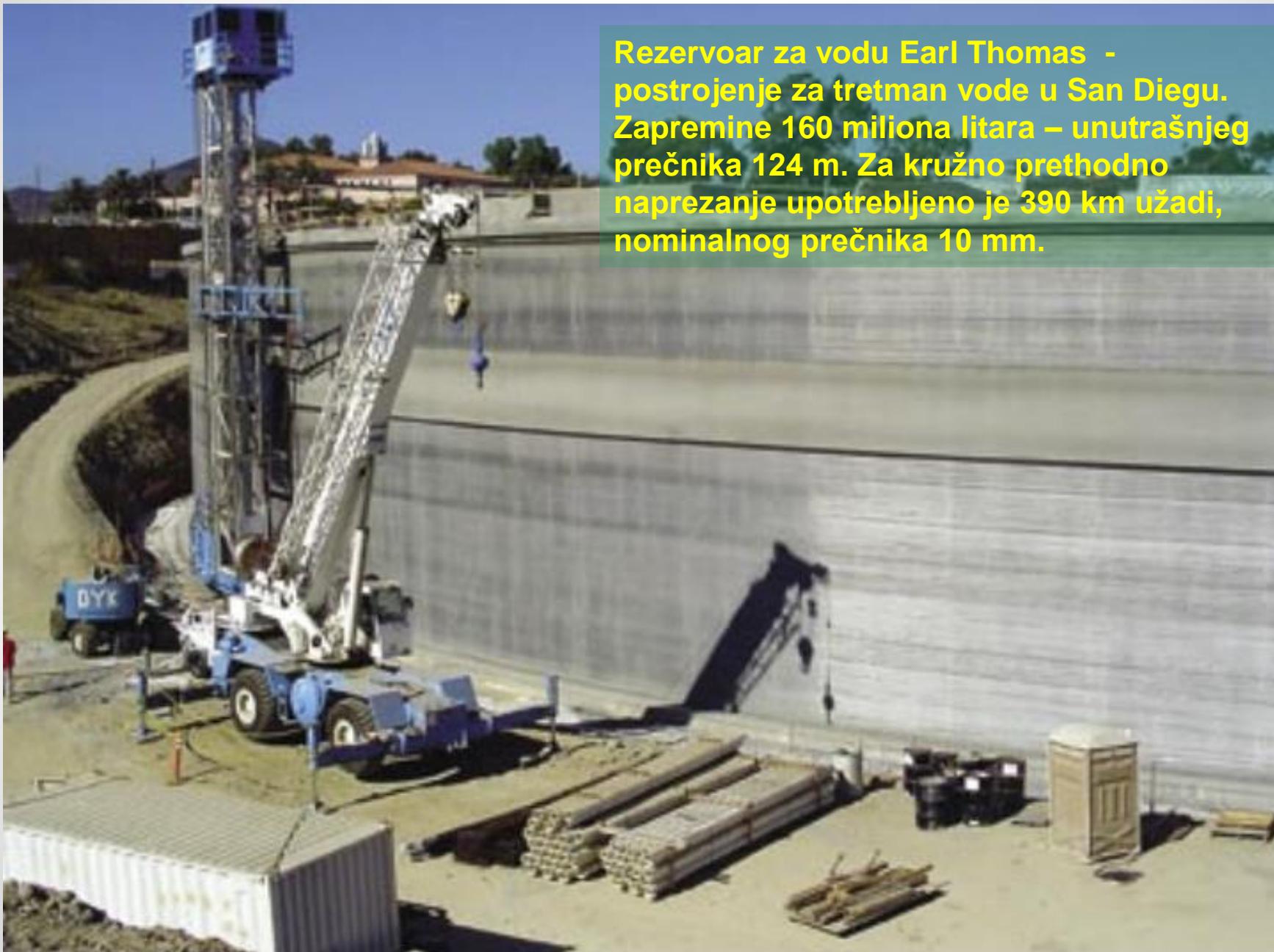
Miješalica sa pumpom za injektiranje



Hidraulična presa za zatezanje šipki

Primjena prethodnog naprezanja

Rezervoari



Rezervoar za vodu Earl Thomas - postrojenje za tretman vode u San Diegu. Zapremine 160 miliona litara – unutrašnjeg prečnika 124 m. Za kružno prethodno naprezanje upotrebljeno je 390 km užadi, nominalnog prečnika 10 mm.

Silosi



Prethodno naprezanje silosa - spolja



Silos za cement u Kataru

Raspone konstrukcije mostova



A10 Arruda dos Vinhos,
Portugal

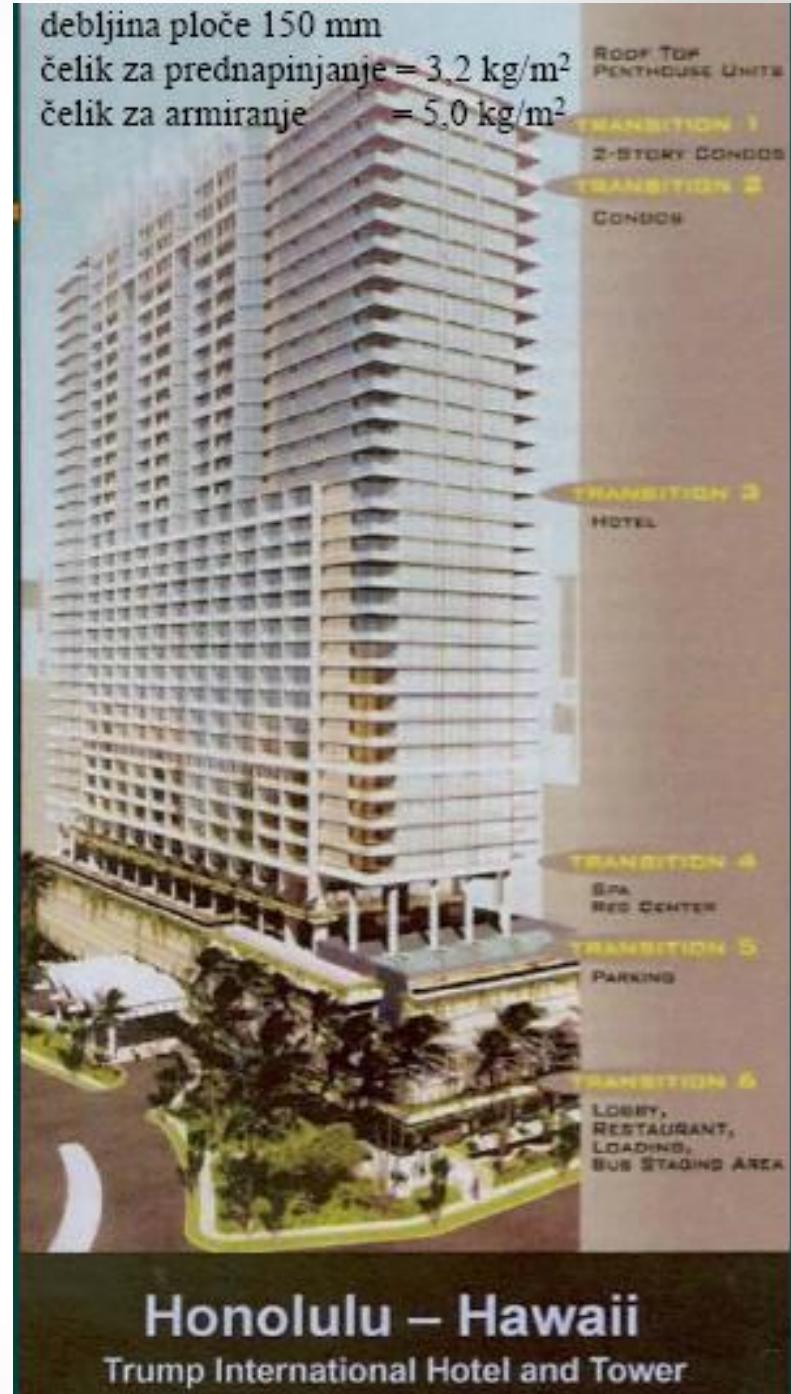


Uhlava Bridge, Pilsen, Czech Republic

Visoke zgrade



Post-Tower, Bonn, Germany



Honolulu – Hawaii
Trump International Hotel and Tower

Zgrada Nacionalne banke u Abu Dabiju



Zgrada Evropskog Parlamenta u Strazburu

Prethodnim naprezanjem je redukovana
debljina tavanica, obezbijeđena stabilnost i
seizmička otpornost i optimizovan slobodan
raspon.



Prestižna poslovna zgrada Esso Glen u centru Londona gdje je izrađeno 50000m^2 prethodno napregnutih tavanica.



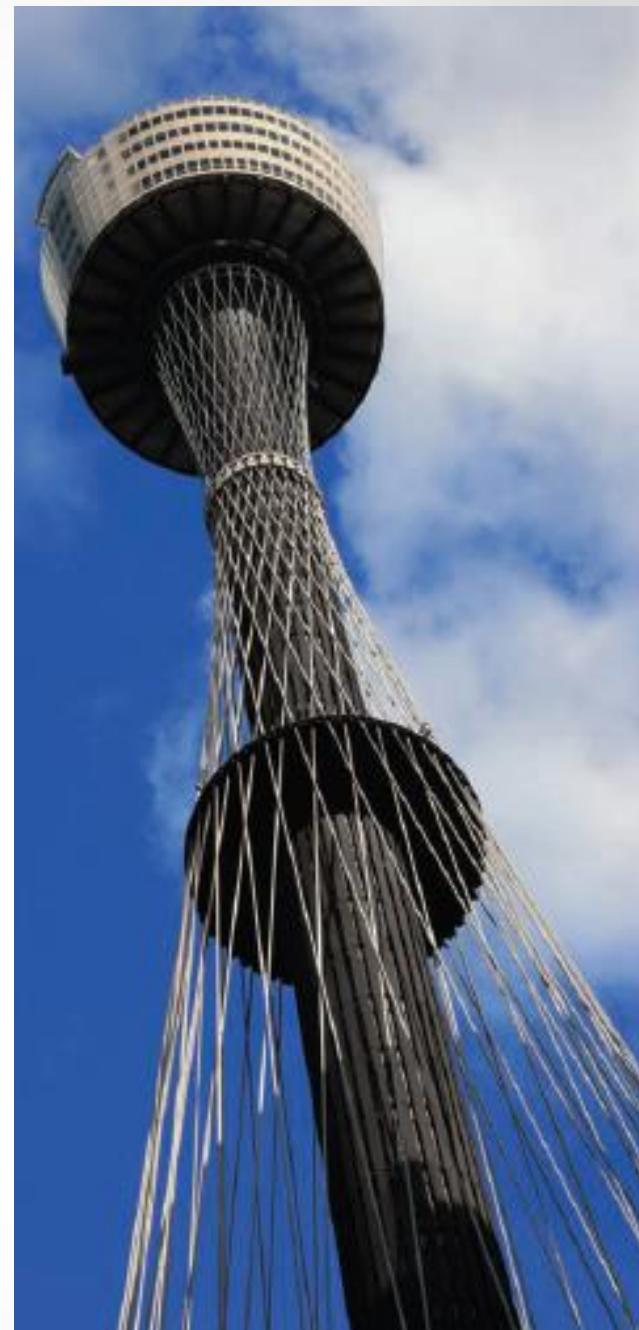
72000m² prethodno napregnutih tavanica je izrađeno pri gradnji fabrike za tretman vode (Vilvoorde, Belgium)

Temelji i hidrotehničke građevine



Cable-stayed sistem se primjenjuje za:

- ✓ Viseće mostove (cable-stayed)
- ✓ Lučne mostove
- ✓ Krovove (stadioni, avionski hangari)
- ✓ Tornjeve (telekomunikacione i sl.)



Cable-stayed



On the Moraca River

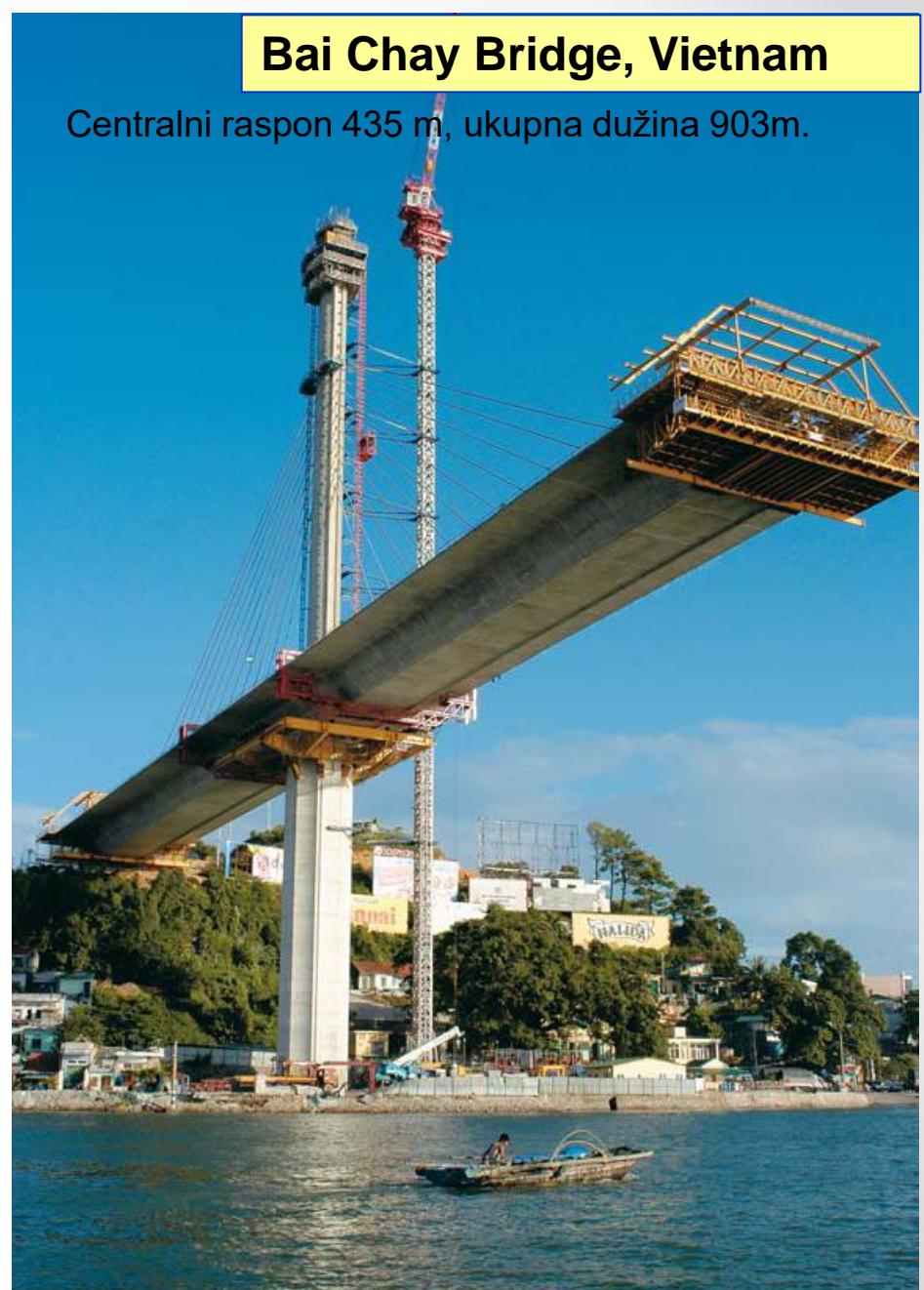
Montenegro. After commencing in May 2005, the installation of the stay cables on the Millennium Bridge, near Podgorica, was completed at the beginning of the summer and the structure was inaugurated on 13 July last. Freyssinet supplied the stay cables (300 t) for the structure, which crosses the Moraca River with a span of 173 m and supervised their installation by the general contractor as part of its role as technical support provider, 1).



1)Soils & Structures, Second half of 2005

Bai Chay Bridge, Vietnam

Centralni raspon 435 m, ukupna dužina 903m.



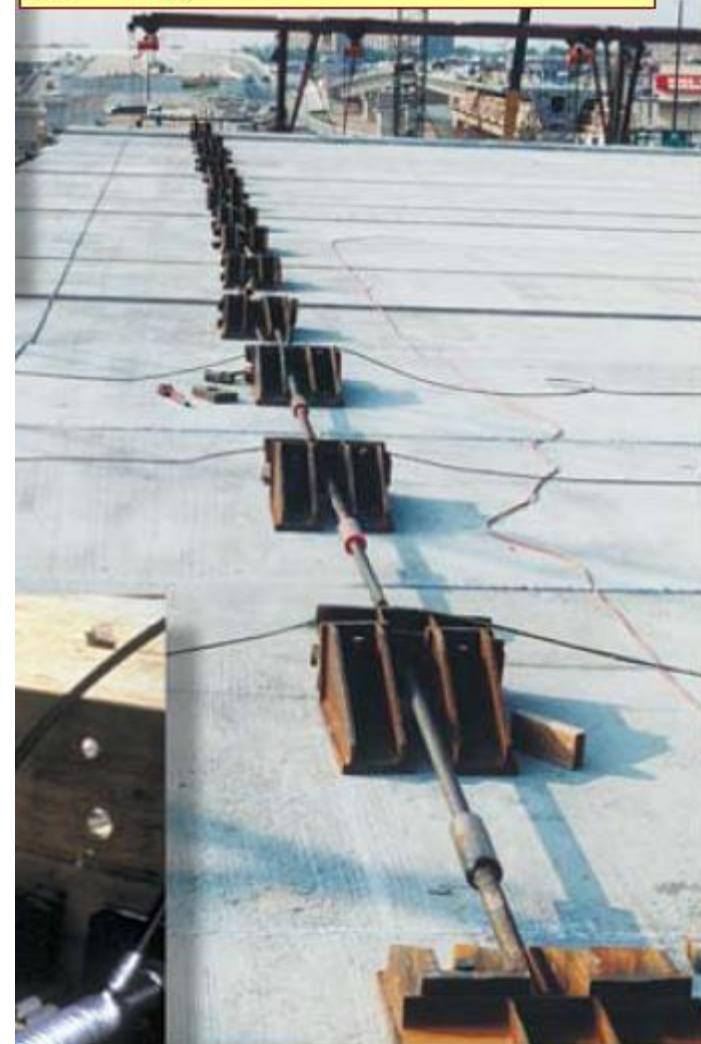
Segmentna gradnja

Most u izgradnji, od prefabrikovanih segmenata, koji se povezuju prethodnim naprezanjem

New Victory
Bridge,
Perth Amboy,
NJ



Privremeno postavljene
šipke pri segmentnoj
gradnji





Most na autoputu u Maroku

Građen je od segmenata livenih na licu mesta uz primjenu prethodnog naprezanja.



Most na autoputu u Mađarskoj

Prethodno napregnut kablovima, sa 17 raspona: $60+95+13 \times 120 + 95+60$; građen metodom konzolne gradnje.

Prefabrikovani prethodno napregnuti elementi



Šuplje ploče



Željeznički pragovi